

Experimental Investigation and Modelling of Hazardous Incidents in Liquid Helium Cryostats

Carolin Heidt KSETA Plenary Workshop 2016, Durbach

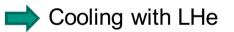
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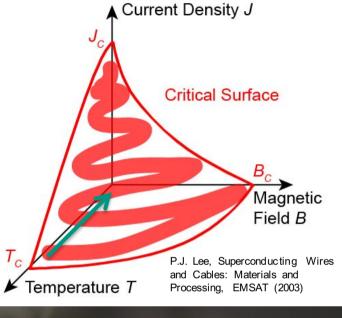
Motivation: Superconductivity

- Conventional conductors: el. resistance → heat → large energy losses
- Superconductors \rightarrow materials with $R = 0 \Omega$ for low J, B, T
- Application: sc. cables, sc. magnets
 - For $J \uparrow, B \uparrow \to T \downarrow$











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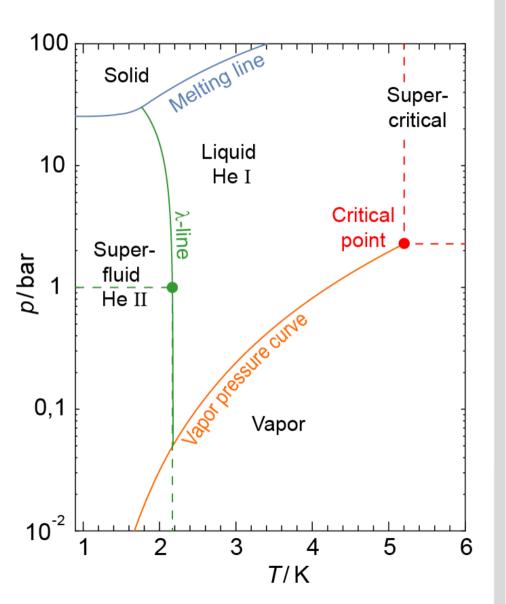
Karlsruhe Institute of Technology

Motivation: Helium

- Two stable isotopes: ³He and ⁴He
- Normal boiling point $T_{\rm nb} = 4.2$ K
- Lowest critical point of all fluids:
 - T_c = 5.195 K
 - $p_{\rm c} = 2.27$ bar
- No solid state at any temperature at p < 25 bar</p>
- Superfluid at $T < T_{\lambda}$

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- $T_{\lambda}(1 \text{ bar}) = 2.17 \text{ K}$
- Enthalpy of evaporation $\Delta h_V(4.2 \text{ K}; 1 \text{ bar}) = 2.6 \text{ kJ/l}$
 - Factor 835 lower than water
 - Factor 62 lower than nitrogen



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Motivation: Incident LHC 09/2008



- Quench of sc. connection → electrical arc → puncture of helium enclosure → vacuum breakdown
- Safety devices too small → damage by overpressure
- Delay >1year, costs several million €









Sources:

http://press.web.cern.ch/pr ess-releases/2008/10/cernreleases-analysis-lhcincident

https://cds.cern.ch/record/1 185822



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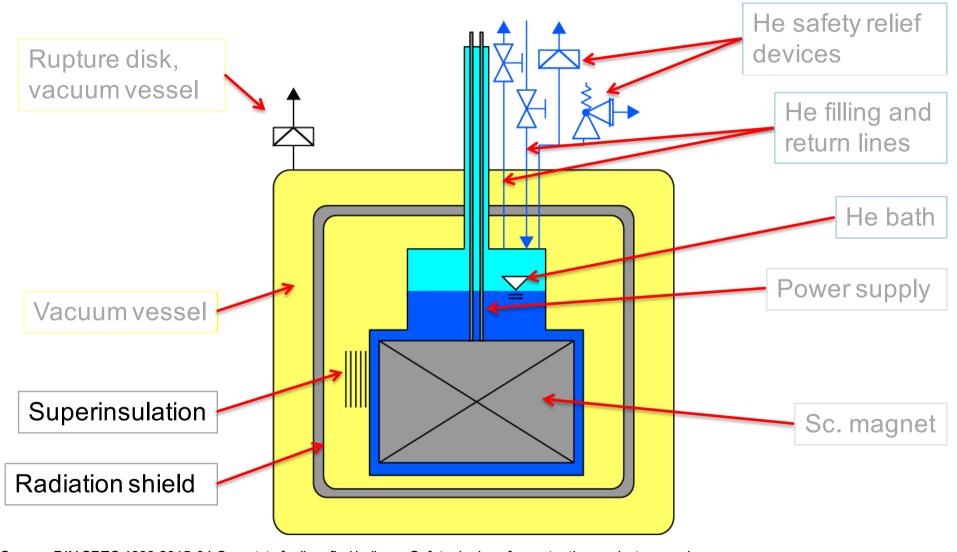
Motivation: Helium Safety





Helium Bath Cryostat



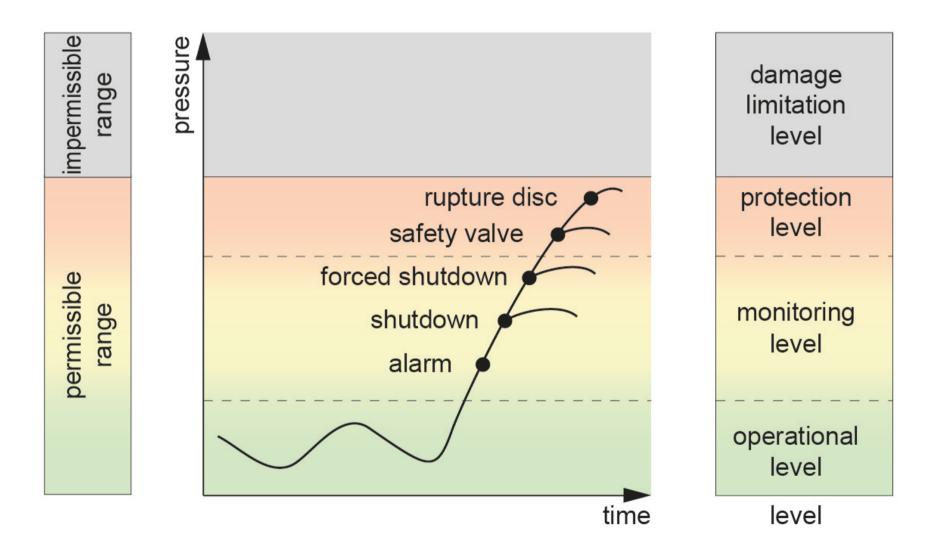


Source: DIN SPEC 4683:2015-04 Cryostats for liquefied helium – Safety devices for protection against excessive pressure

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Safety Concept



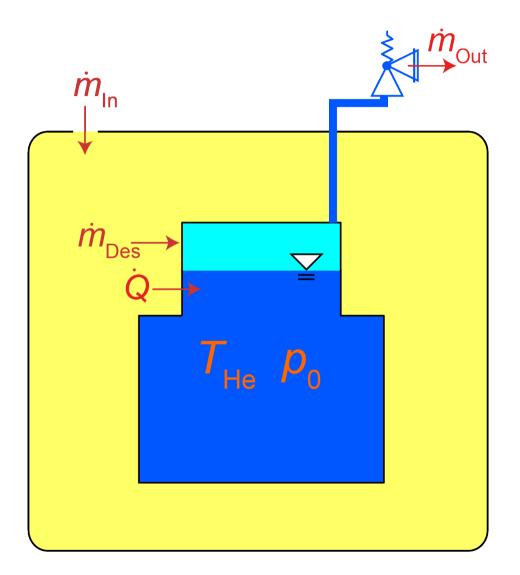


Source: DIN SPEC 4683:2015-04 Cryostats for liquefied helium – Safety devices for protection against excessive pressure

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Example Hazardous Incident





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Dimensioning of cryogenic safety relief devices



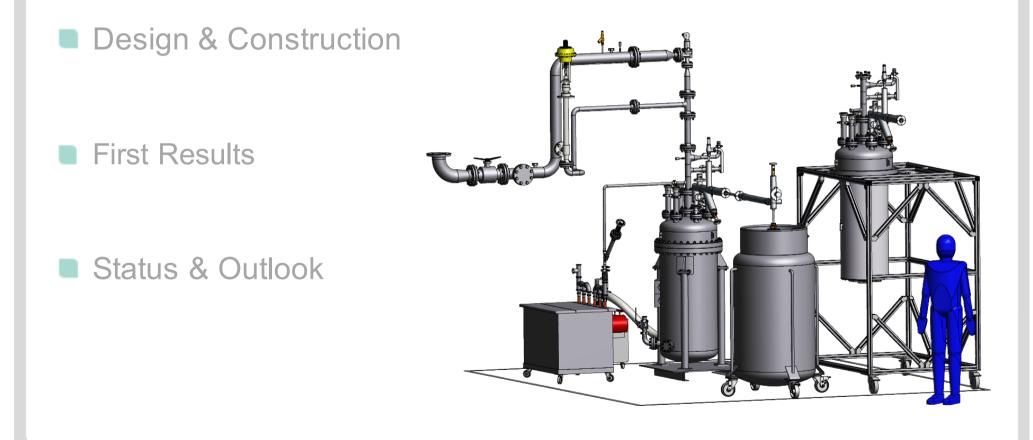
- Dimensioning for worst case: venting of insulating vacuum with atmospheric air
- Existing models and standards (e.g. DIN EN 13648) do not consider **process dynamics** $\rightarrow \dot{q} = \text{const.}$ [1]
 - Oversizing of safety valves
 - Implications on spending, space and helium leakage
- **Dynamic model** links all time-dependent sub-processes [2]
 - ODE system based on thermodynamic and fluid mechanic principles
 - Contains some simplifications (desublimation, kinetics)
 - Experiments for validation and extension of model \rightarrow fit parameters

Lehmann, W., Zahn, G., Safety aspects for LHe cryostats and LHe transport containers, 1987 Proc. Int. Cryog. Eng. Conf. 7 569-579
 Heidt, C., Grohmann, S., Süßer, M., Modeling the Pressure Increase in Liquid Helium Cryostats after Failure of the Insulating Vacuum, 2014 AIP Conf. Proc. 1573 1574-1580



PICARD

Purpose & Operating Range



Purpose & Operating Range PICARD



- Test facility PICARD: Pressure Increase in Cryostats and Analysis of Relief Devices
 - Cryogenic liquid volume: **100 liters**
 - Nominal design pressure: **16 bar(g)**
 - Helium discharge mass flow rates: up to about 4 kg/s
- Broad range of experiments with cryogenic fluids in cooperation with CERN [3]
 - Heat flux and flow rate measurements under various conditions
 - Studies on the impact of **two-phase flow**
 - Measurement of **flow coefficients** of safety devices at 4...300 K

[3] Collaborative R&D on experimental testing on cryogenic pressure relief between CERN and KIT, KE2974/KT/DGS/222C, 12/2015

Purpose & Operating Range

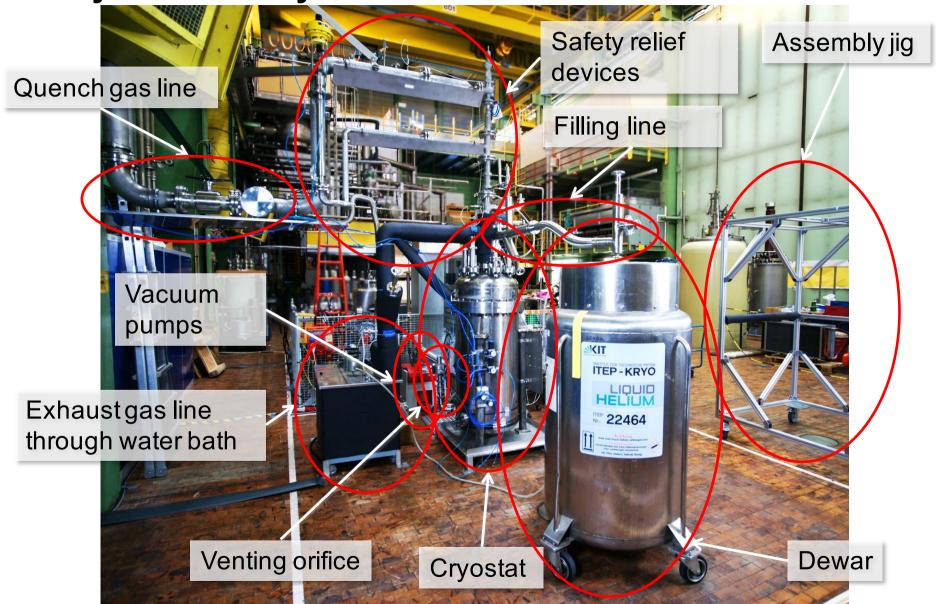


Variation of	Range
Venting diameter	140 mm
Insulation	030 layers of superinsulation, with/without radiation shield
Liquid level	2080 %

[4] Heidt, C., Schön, H., Stamm, M., Grohmann, S., Commissioning of the cryogenic safety test facility PICARD, 2015, *IOP Conf. Ser.: Mater. Sci. Eng.* **101**, 012161

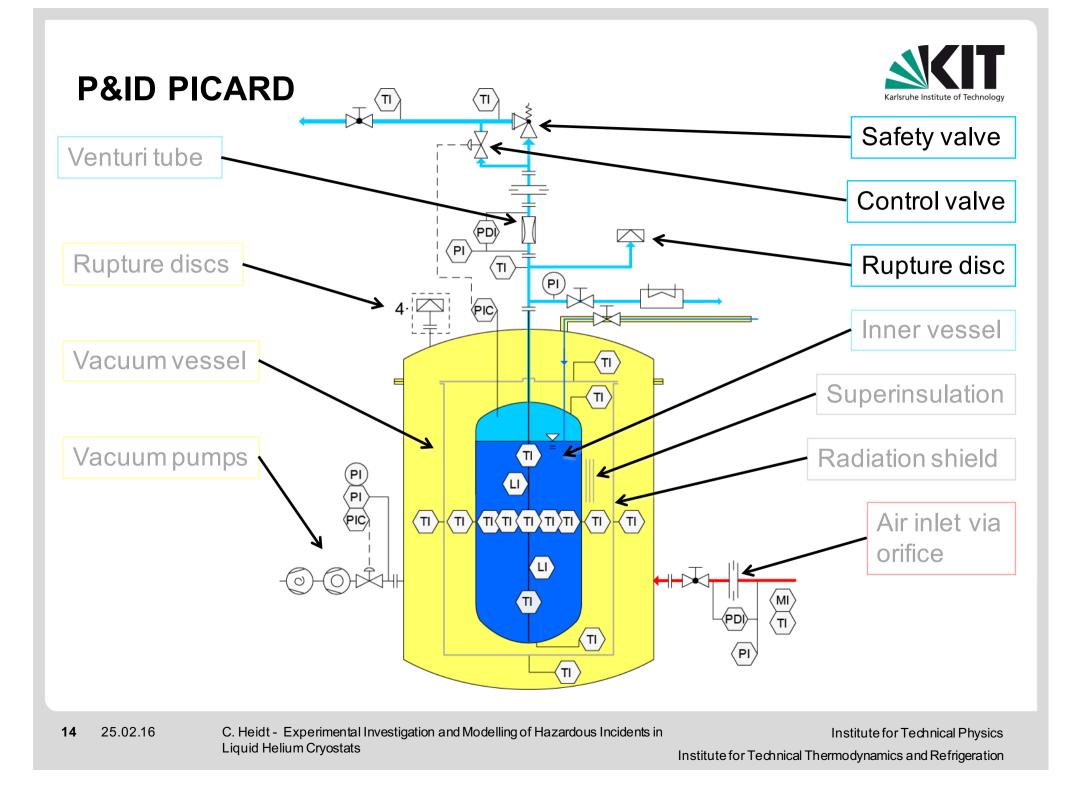
Safety Test Facility PICARD

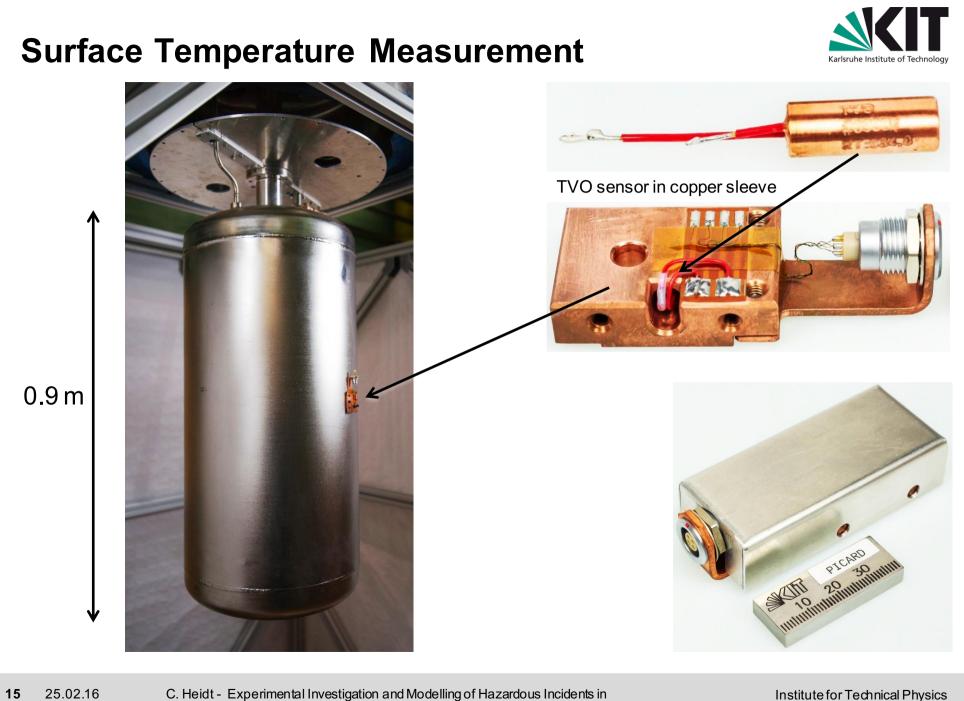




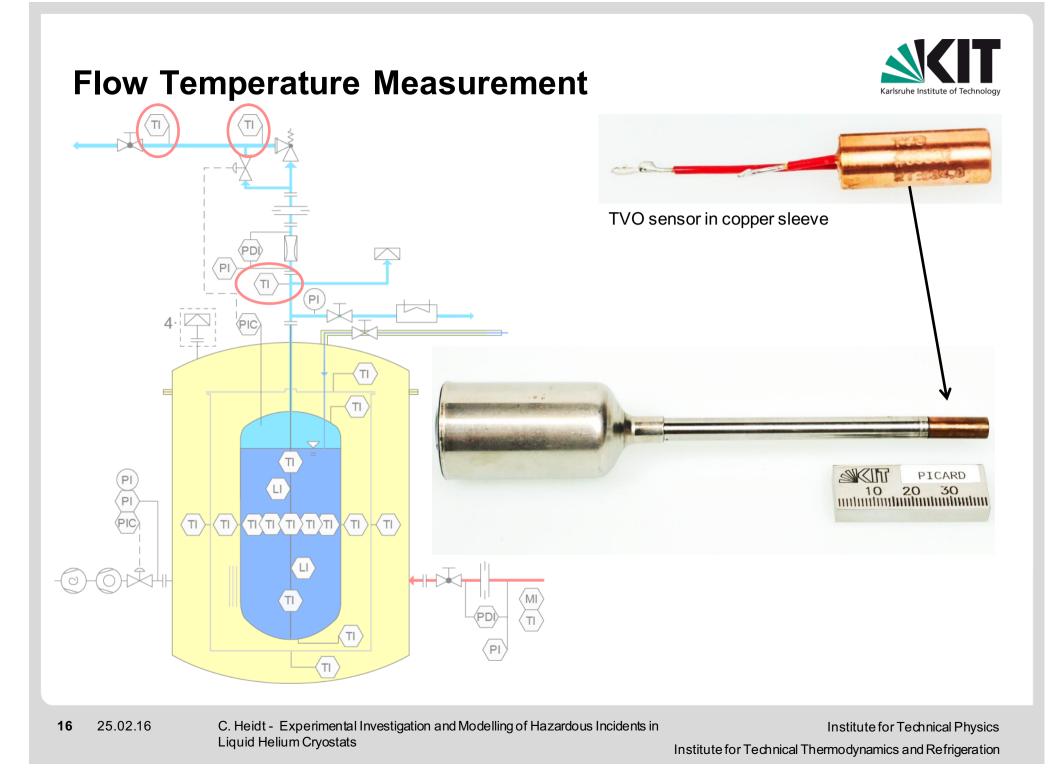
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Liquid Helium Cryostats



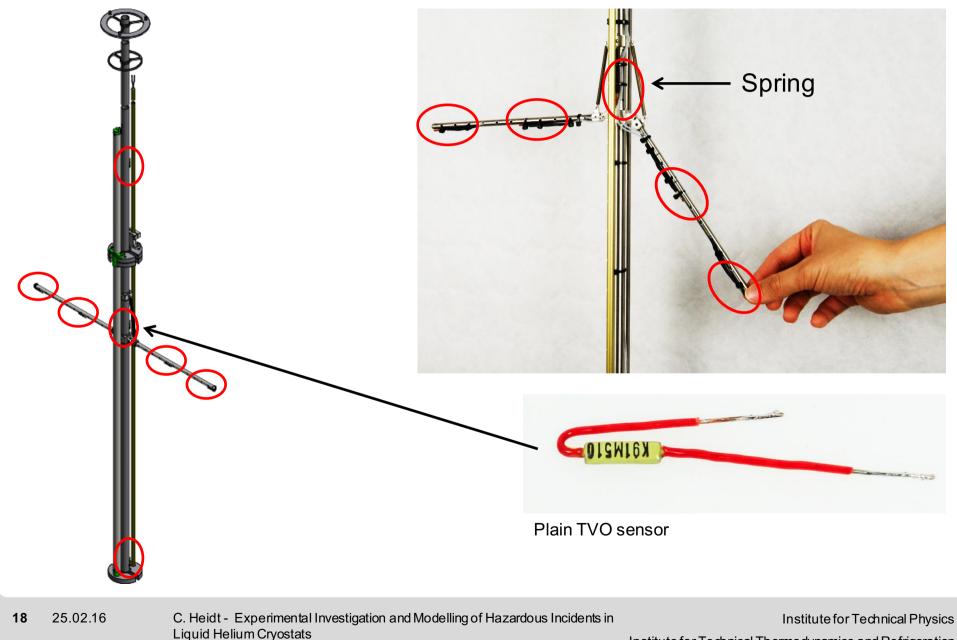
Fast Temperature Measurement Karlsruhe Institute of TI PICARD PI PI TI TI PI ΤΙζΤΙζΤΙΣΤΙΣΤΙ TI (TI) TI M (TI) ТΙ 17 25.02.16

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Fast Temperature Measurement

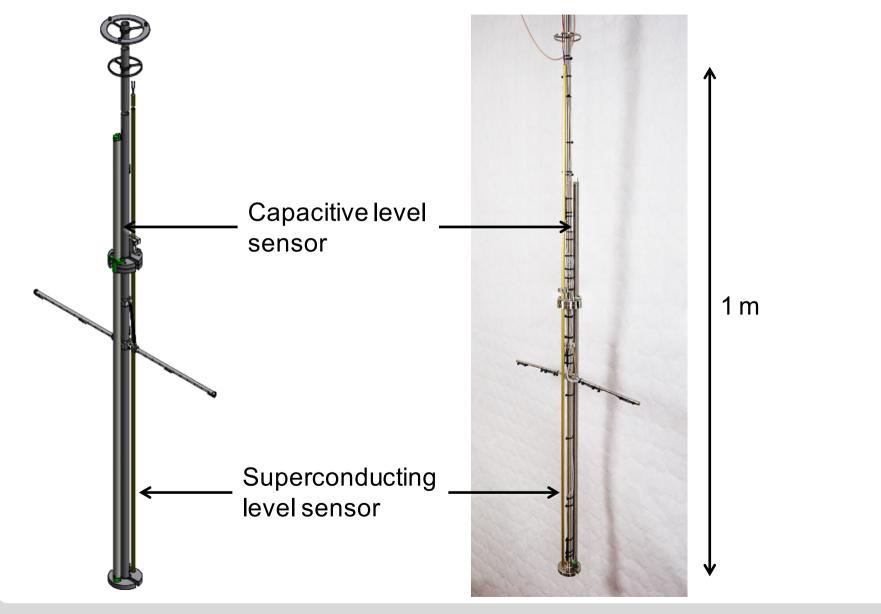




Level Measurement

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PICARD

Purpose & Operating Range

Design & Construction
First Results
Status & Outlook

0.5 Venting with atmospheric air 0.4 Venting diameter: 12.5 mm Massflow in kg/s 0.2 0.1 Set pressure safety valve: 2 barg Closed Open Filling level: ~50% Liquid He volume: 591 0.0 5 10 15 20 pressure impermissible 4 Time in s range p₀+50% 3 Pressure in barg rupture disc p_+10% safety valve 2 \mathbf{p}_0 forced shutdown permissible range shutdown alarm 00 5 10 15 20 Time in s time

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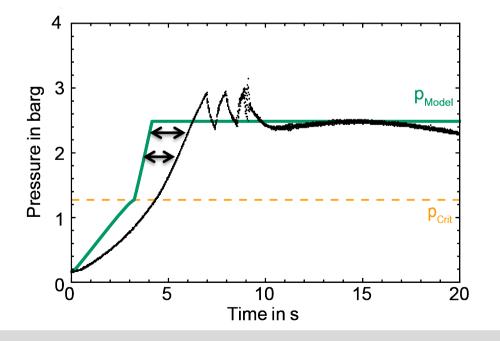
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Results of First Venting Experiments

Results of First Model Fitting

- Venting with atmospheric air
- Venting diameter: 12.5 mm
- Set pressure safety valve: 2 barg
- Filling level: ~50%
- Liquid He volume: 591
- Set pressure model: 2.5 barg
- Desublimation fittet → absolute values correspond well
- Time difference → heat transmission resistance



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Status & Outlook PICARD



- Design & Construction
- 🛢 Commissioning 🗸
 - Pressure and leak test
 - Instrumentation
- Experiments
 - Venting with nitrogen and air
 - Small venting diameters
 - Low set pressures
 - Without superinsulation
- Parameter fit model
 - Desublimation
 - Kinetics √

- Planned experiments:
 - Larger venting diameters
 - Higher set pressures
 - With other cryogenic fluids
 - Simulation of magnet quench
- Investigation of
 - Safety valve behavior at cryogenic temperatures
 - Two-phase flow

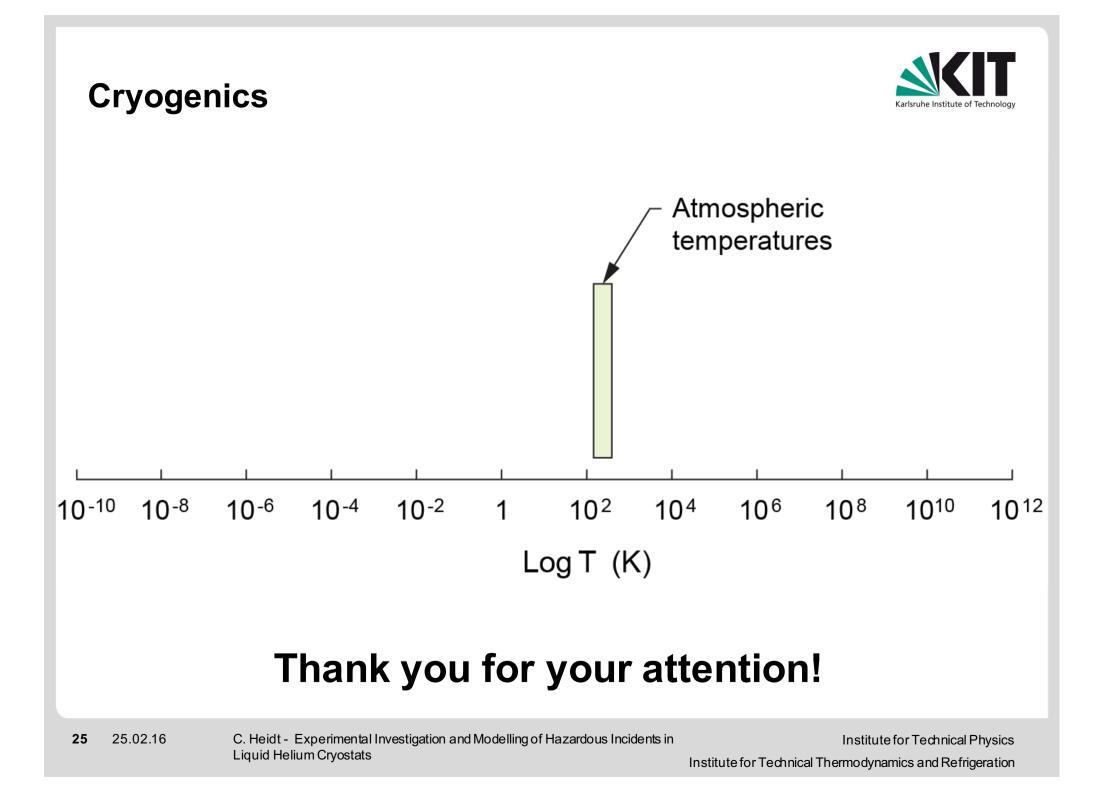
Outlook?

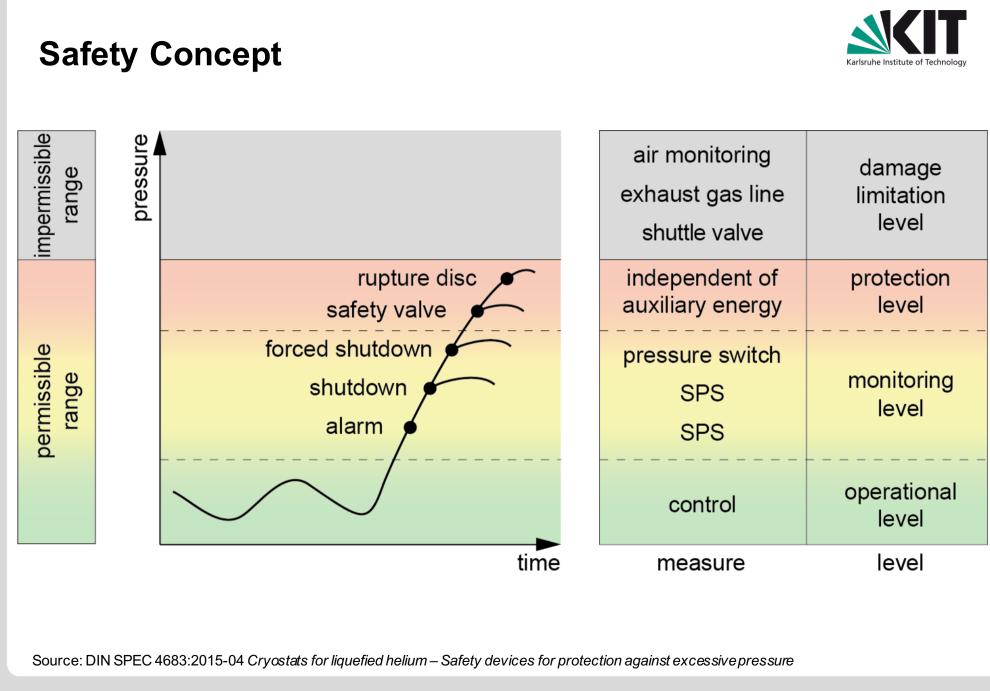


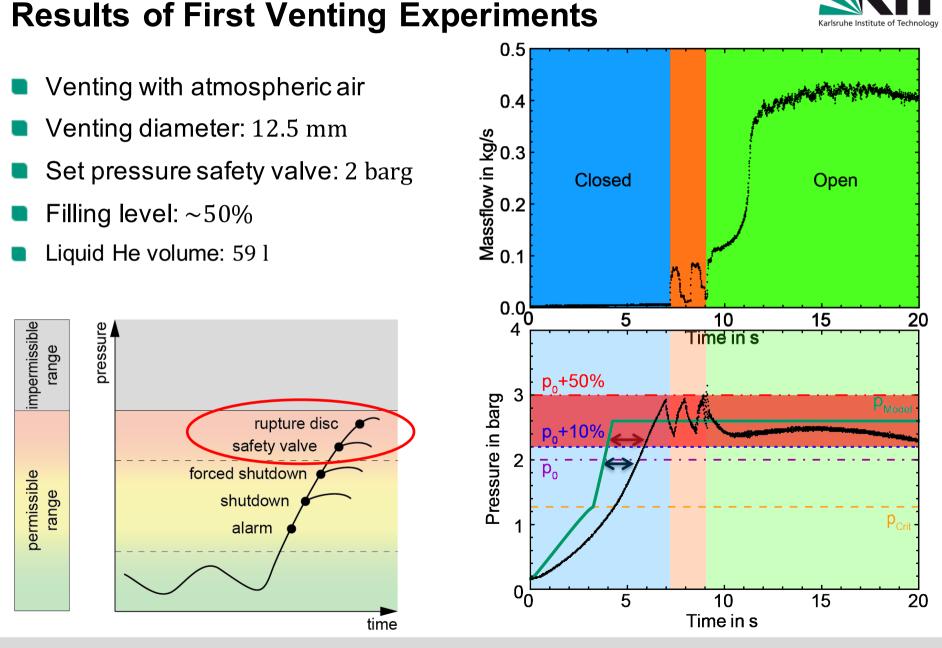


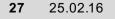
Citation: IMDb, Quotes for Captain Jean-Luc Picard (Character) from Star Trek: The Next Generation (1987), Star Trek - Nemesis (2002), Paramount Pictures, http://www.imdb.com/character/ch0001449/quotes-access: 2015/08/13 Pictures: www.moviepilot.de

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Thank you for your attention!

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Dimensions PICARD



Component	Parameter	Value
Inner vessel	Height	900 mm
	Diameter	400 mm
	Typical liquid volume	100 I
	Nominal pressure	16 bar(g)
Outer vessel	Height	1500 mm
	Diameter	600 mm
	Nominal pressure	10 bar(g)
Radiation shield	Height	1050 mm
	Diameter	500 mm
Vent line	Diameter	60 mm
Quench gas line	Diameter	100150 mm

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Expected Mass Flow Rates



- Calculation based on [3]

Set pressure of relief device in bar (abs)	Expected mass flow in kg/s
3	3.3
5	2.3
8	1.7
10	1.5



- With 10 layers of superinsulation
- **a** $\dot{q} = 0,6 \text{ W/cm}^2 [1]$
- Calculation based on [3]

Set pressure of relief device in bar (abs)	Expected mass flow in kg/s
3	0.51
5	0.37
8	0.27
10	0.23

[1] W. Lehmann, and G. Zahn, "Safety aspects for LHe cryostats and LHe containers", in PROC INT CRYOG ENG CONF, London, 1978, vol. 7, pp. 569–579

[3] Varghese, A. P., Zhang, B. X., "Capacity requirements for pressure relief devices on cryogenic containers", in *ADV CRYOGEN ENG*, Huntsville, Alabama, 1991, Vol. 37, pp. 1487–1493

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Vacuum Space: Ideal gas law $p_{\rm V}(\tau)$ Fluid mechanics Fluid property data . ṁ_{оut} **Transition:** Desublimation $\dot{Q}(au)$ $\dot{m}_{_{Des}}$ **Kinetics Inner Vessel:** ، ش_{ام} Isochoric process First law of thermodynamics $T_A^{}, p_A^{}$ p_{He}, He' Fluid property data $p_{\rm He}(\tau), T_{\rm He}(\tau)$ Isobaric process First law of thermodynamics $A_{He,}^{\setminus}T_{W}$ Fluid mechanics Fluid property data Simultaneous numeric solution of ODEs

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Model Development & Solution

