Experimental & Modelling Digital Twin Approach for Polymer Synthesis via Re-initiated Oxygen inhibited RAFT Polymerization

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Introduction

Controlled polymerization techniques like the reversible-addition fragmentation chain transfer polymerization (RAFT) are sensitive to impurities such as oxygen [1]. In this work, a kinetic model describing the oxygen inhibited RAFT dispersion polymerization for the synthesis of poly(4-vinylpyridine)-b-polystyrene (P4VP-b-PS) [2-3] is developed and using the model, the effect of the re-initiation on the inhibited RAFT polymerization is predicted. Based on the prediction, re-initiation is applied as a tool to enhance monomer conversion, which leads to:

- More sustainable polymerisation process
- Prevention of loss of valuable material
- Easier purification of final product



Figure 1. Digital twin approach for polymer synthesis via re-initiated oxygen-inhibited RAFT polymerization. [1]

Modeling Approach

Literature

Table 1. Kinetic model describing reaction steps of inhibition process. [1]

Inhibition by Oxygen

$$\begin{split} P_n^* + O_2 \xrightarrow{k_{in,O_2,1}} P_n(O_2)_1^* \\ P_n(O_2)_l M^* + O_2 \xrightarrow{k_{in,O_2,1}} P_{n+1}(O_2)_{l+1}^* \\ P_n(O_2)_l M^* + M \xrightarrow{k_p} P_{n+1}(O_2)_l M^* \\ P_n(O_2)_l^* + M \xrightarrow{k_{in,O_2,2}} P_n(O_2)_l M^* \\ P_{n_1}(O_2)_{l_1}^* + P_{n_2}(O_2)_{l_2}^* \xrightarrow{k_{in,O_2,3}} M_{n_1}(O_2)_{l_1-1} OH + M_{n_2}(O_2)_{l_2-1} = O + O_2 \\ P_{n_1}(O_2)_{l_1}^* + P_{n_2}(O_2)_{l_2} M^* \xrightarrow{k_{td}} M_{n_1}(O_2)_{l_1-1} + M_{n_2}(O_2)_{l_2} M \\ P_{n_1}(O_2)_{l_1}^* + P_{n_2}(O_2)_{l_2} M^* \xrightarrow{k_{td}} M_{n_1}(O_2)_{l_1} + M_{n_2} \\ P_{n_1}(O_2)_{l_1} M^* + P_{n_2} \xrightarrow{k_{td}} M_{n_1}(O_2)_{l_1} M + M_{n_2} \\ P_{n_1}(O_2)_{l_1} M^* + P_{n_2}(O_2)_{l_2} M^* \xrightarrow{k_{td}} M_{n_1}(O_2)_{l_1} M + M_{n_2} \\ P_{n_1}(O_2)_{l_1} M^* + P_{n_2}(O_2)_{l_2} M^* \xrightarrow{k_{td}} M_{n_1}(O_2)_{l_1} M + M_{n_2} \\ P_{n_1}(O_2)_{l_1} M^* + P_{n_2}(O_2)_{l_2} M^* \xrightarrow{k_{td}} M_{n_1}(O_2)_{l_1} M + M_{n_2} \\ P_{n_1}(O_2)_{l_1} M^* + P_{n_2}(O_2)_{l_2} M^* \xrightarrow{k_{td}} M_{n_1}(O_2)_{l_1} M + M_{n_2} \\ P_{n_1}(O_2)_{l_1} M^* + P_{n_2}(O_2)_{l_2} M^* \xrightarrow{k_{td}} M_{n_1}(O_2)_{l_1} M^* + M_{n_2}(O_2)_{l_2} M \\ \end{pmatrix}$$

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[3] F. Kandelhard, et al., Ind. Eng. Chem. Res., 2023, DOI: 10.1021/acs.iecr.3c00607

Results







Figure 2. Evolution of simulated (dashed line) and experimental (points) styrene conversion X (a) and number average molar mass $\overline{M}_{n,theo}$ (b) within the period of 24 h for three different RAFT : Initiator ratios of 10:1 in oxygen-free solution (\blacksquare), 10:1 (\blacktriangle) and 10:4 (\bullet) in oxygen-exposed solutions. [1]

Parameter Estimation & Model Prediction

Table 2. Results of parameter estimation for the reaction coefficients $k_{in,0_2,1}$, $k_{in,0_2,2}$ and $k_{in,0_2,3}$ are reaction rate coefficient of oxygen molecule with growing radicals at 60 °C, of monomer with peroxy radicals and of the termination of the peroxy radicals, respectively. [1]



Figure 3. Simulated $\overline{M}_{n,theo}$ and X upon re-initiation of the polymerization. [1]

Re-initiation



Figure 4. Evolution of a) styrene conversion and b) dispersity and apparent number average molar mass of the (\blacksquare) oxygen-free initiated and (\blacktriangle) oxygen-free and re-initiated as well as (\bullet) oxygen-exposed and re-initiated experiments. [1]

Summary Model & Re-initiation (>96 %) (>96 %) (>96 %) (>96 %) (>1.2) * Easier purification * Reduction of material waste (>1.2)

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