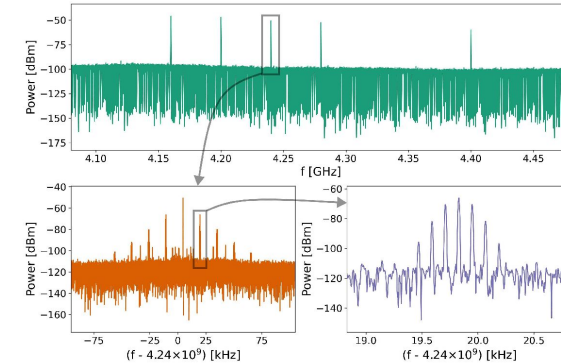
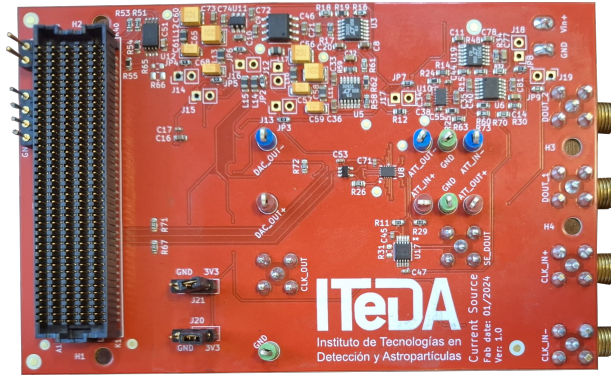


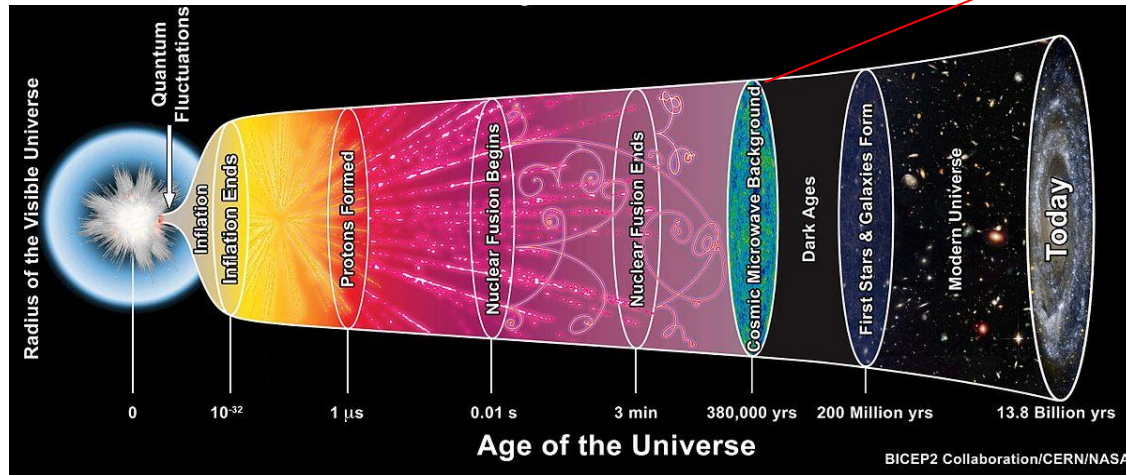
Signal Processing in the Microwave SQUID Multiplexer-based Readout System for Magnetic Microbolometer Detector Arrays

Eng. Juan Manuel Salum

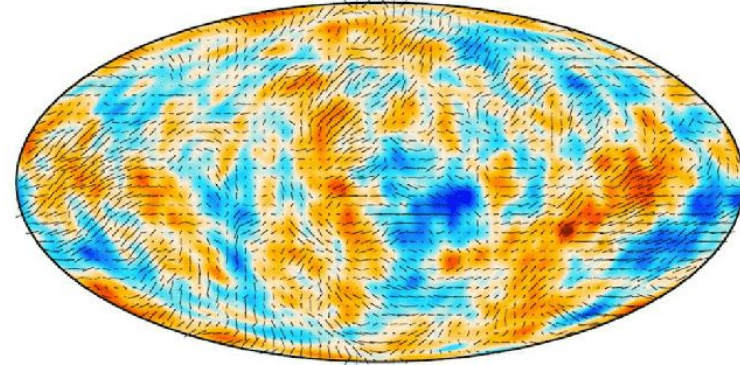


Motivation

Photons propagate freely



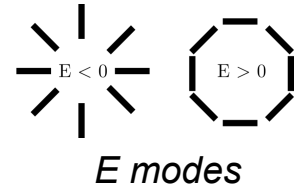
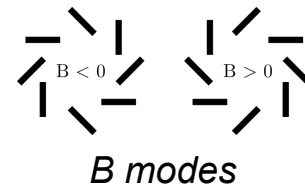
The Cosmic Microwave Background (CMB)



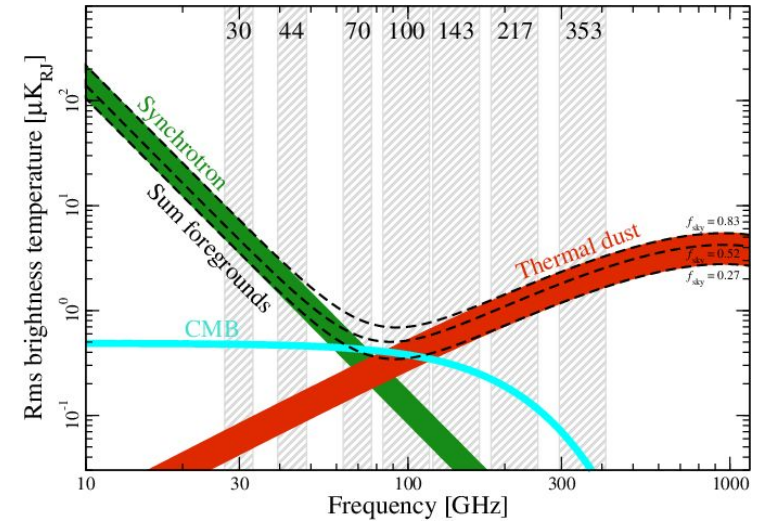
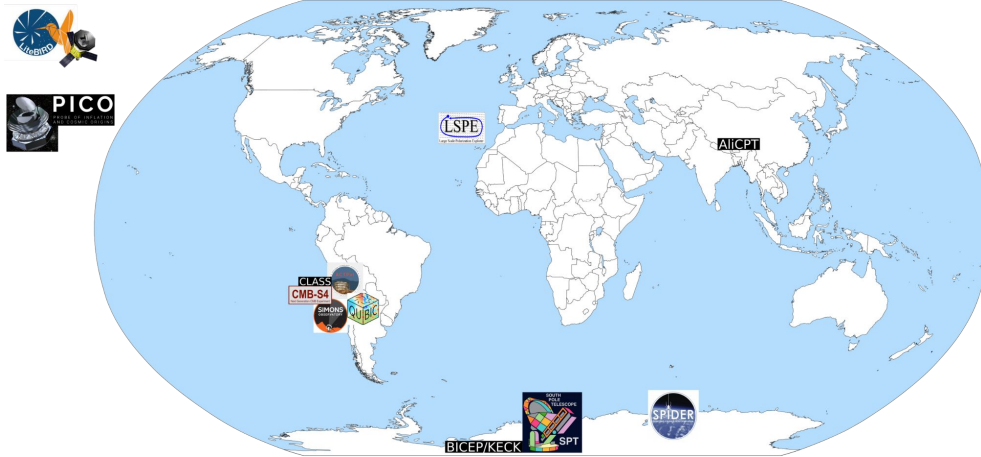
Credits: Planck collaboration

Inflation Theory

- The Universe expanded exponentially, leading to its cooling
- Photons enabled to freely propagate after recombination epoch
- The footprint of this process is in the CMB polarization
- CMB is B- and E-mode polarized
- **Detecting B modes provides direct evidence of the inflationary period**



Challenges for B modes detection



Credits: Planck collaboration

→ Effort by the scientific community to measure B-modes

→ Measurement challenges:

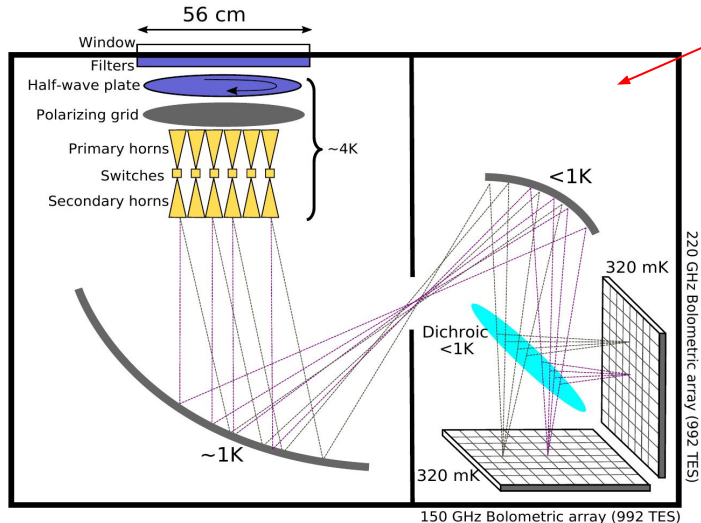
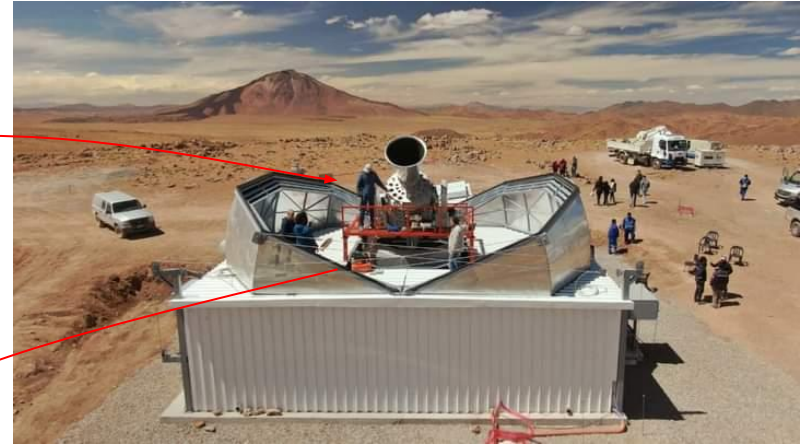
- ◆ B-mode is a weak signal —————> Low-temperature bolometer arrays
- ◆ Foregrounds —————> Additional bands for foregrounds removal
- ◆ Systematic effects —————> Calibration

Bolometric Interferometry

Bolometric Interferometry and QUBIC



The QUBIC telescope

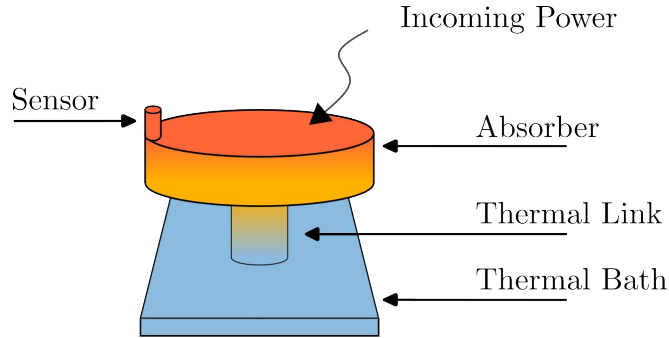


- QUBIC is the first bolometric interferometer for CMB
- Two 1024 bolometer arrays for 150GHz and 220GHz
- Back-to-back horns calibrates the interferometer pattern
- The system is housed in a cryostat at low temperatures to reduce detection noise
- QUBIC challenges:
 - ◆ Designing the dichroic plate for simultaneous 150GHz and 220GHz operation
 - ◆ Readout system scalability

A proposal for QUBIC next generation

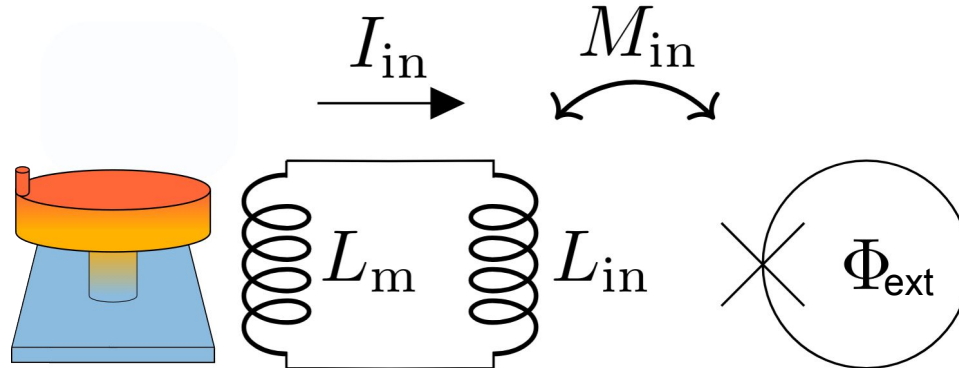
- Multichroic antenna-coupled Magnetic Microbolometer (MMB)
 - ◆ Multiple observation bands in a single pixel avoid the use of the dichroic
 - ◆ Novel detector based on the Magnetic Microcalorimeter (MMC)
- A microwave SQUID multiplexer readout system
 - ◆ Promising technology for high-sensitivity readout
 - ◆ High-multiplexing factor
- Room temperature electronics
 - ◆ A system based on a software-defined radio scheme is proposed due to its adaptability to different experiments requirements
 - ◆ FPGA-based system enables high scalability and flexibility

Novel detector: Magnetic Microbolometer (MMB)



- Photons absorption increase the absorber temperature
- A Au:Er paramagnetic sensor embedded in a magnetic field changes its magnetization with the temperature
- The magnetic flux passing through the sensor changes, generating a measurable signal

MMB readout

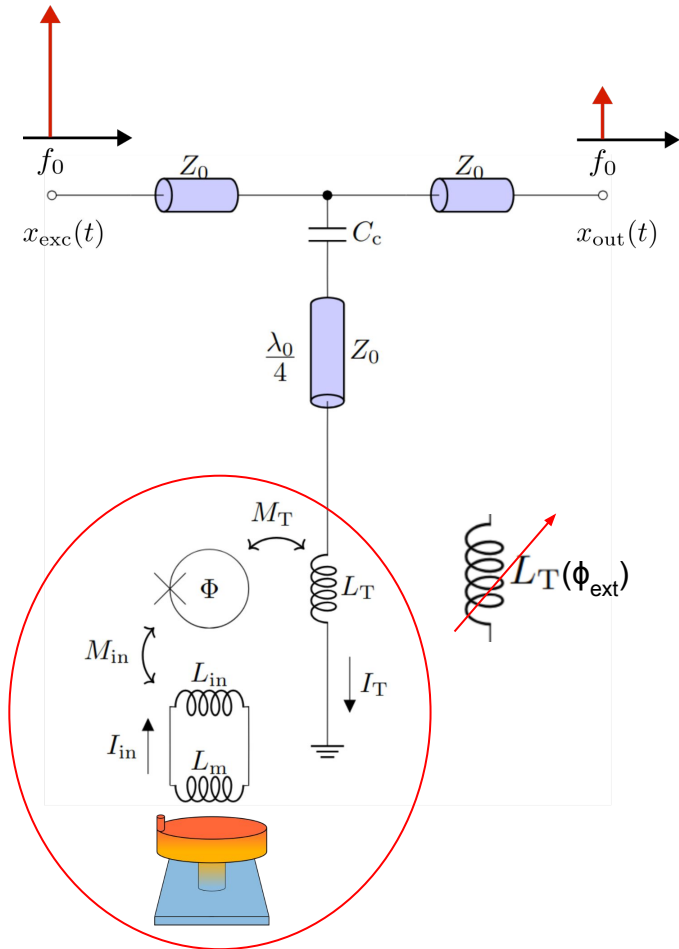


- Magnetic flux is readout with a radio frequency Superconductive Quantum Interference Device (rf-SQUID)
- The supercurrent in the rf-SQUID follows

$$I_s = -I_c \sin \left(\frac{2\pi \Phi_{ext}}{\Phi_0} + \frac{2\pi L_s I_s}{\Phi_0} \right)$$

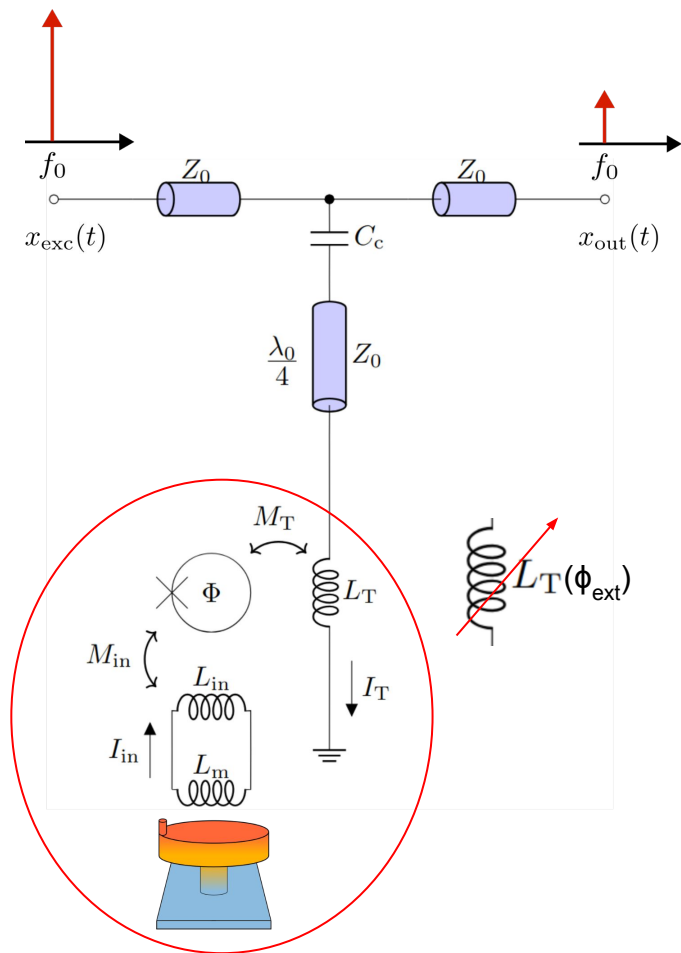
Detector Signal

rf-SQUID readout

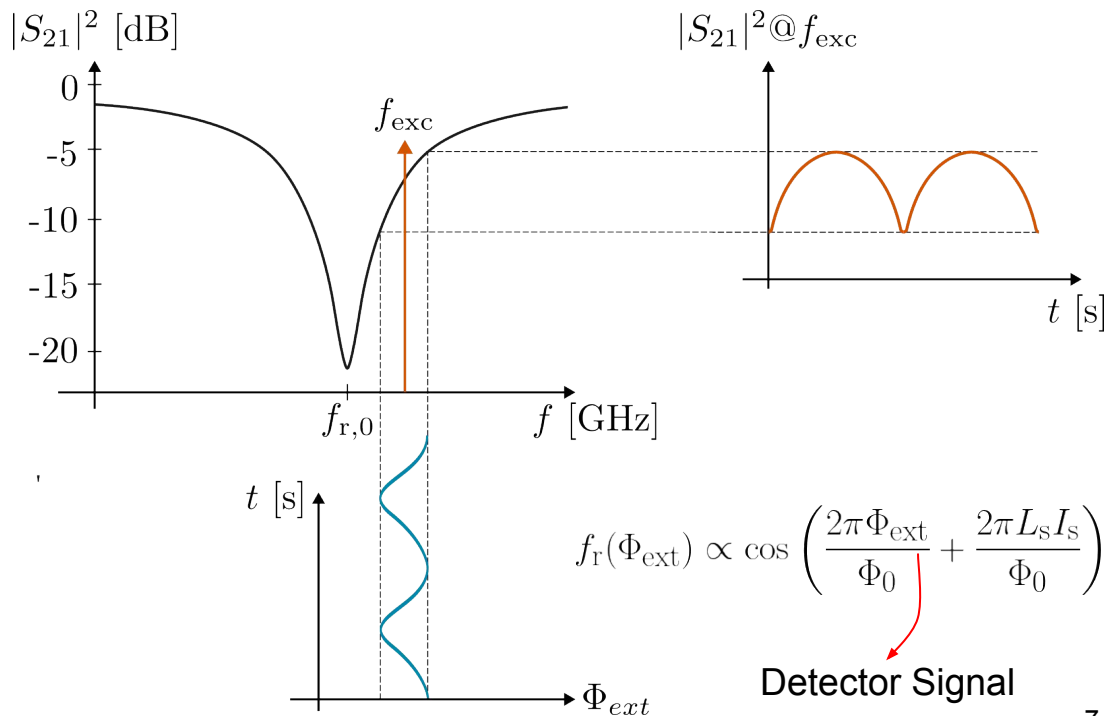


- rf-SQUID coupled to a resonator
- Inductance as a function of external magnetic flux

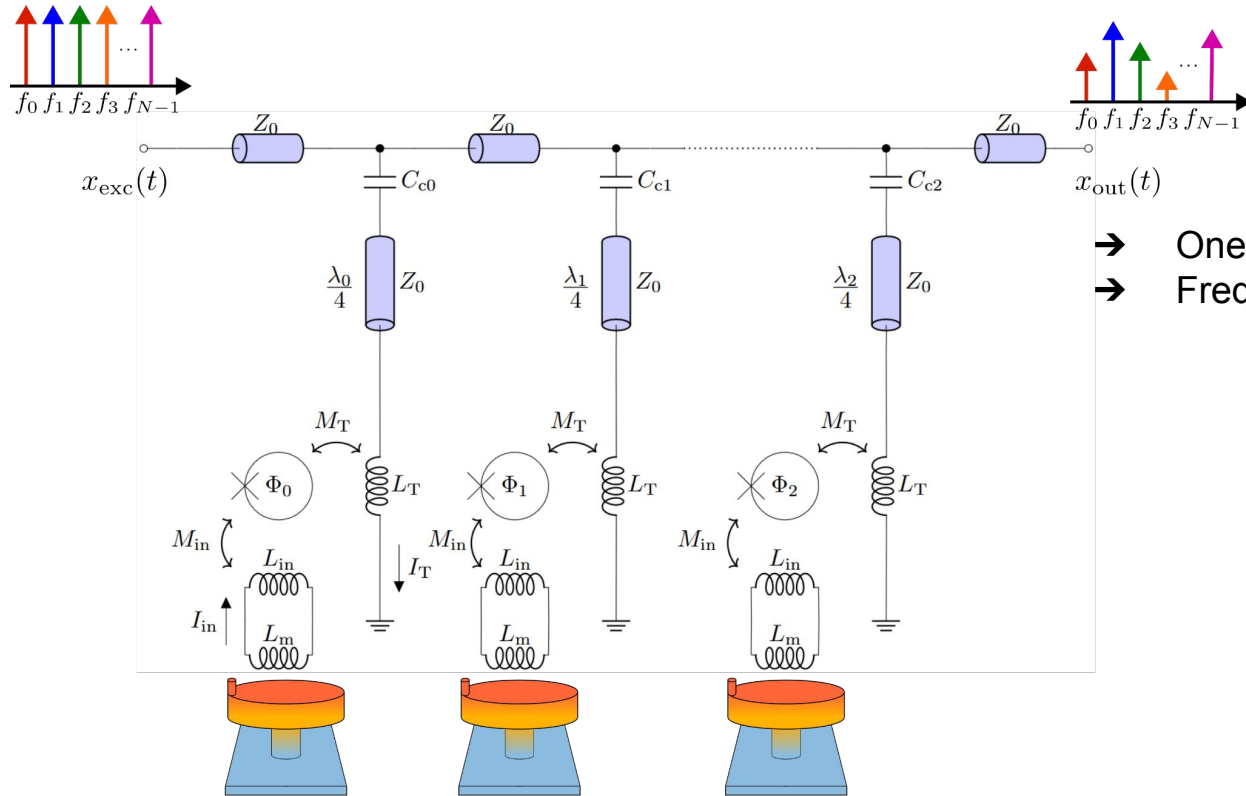
rf-SQUID readout



- rf-SQUID coupled to a resonator
- Inductance as a function of external magnetic flux
- Detector signal shifts the resonator response (s_{21})
- **A readout tone monitors the resonator state**

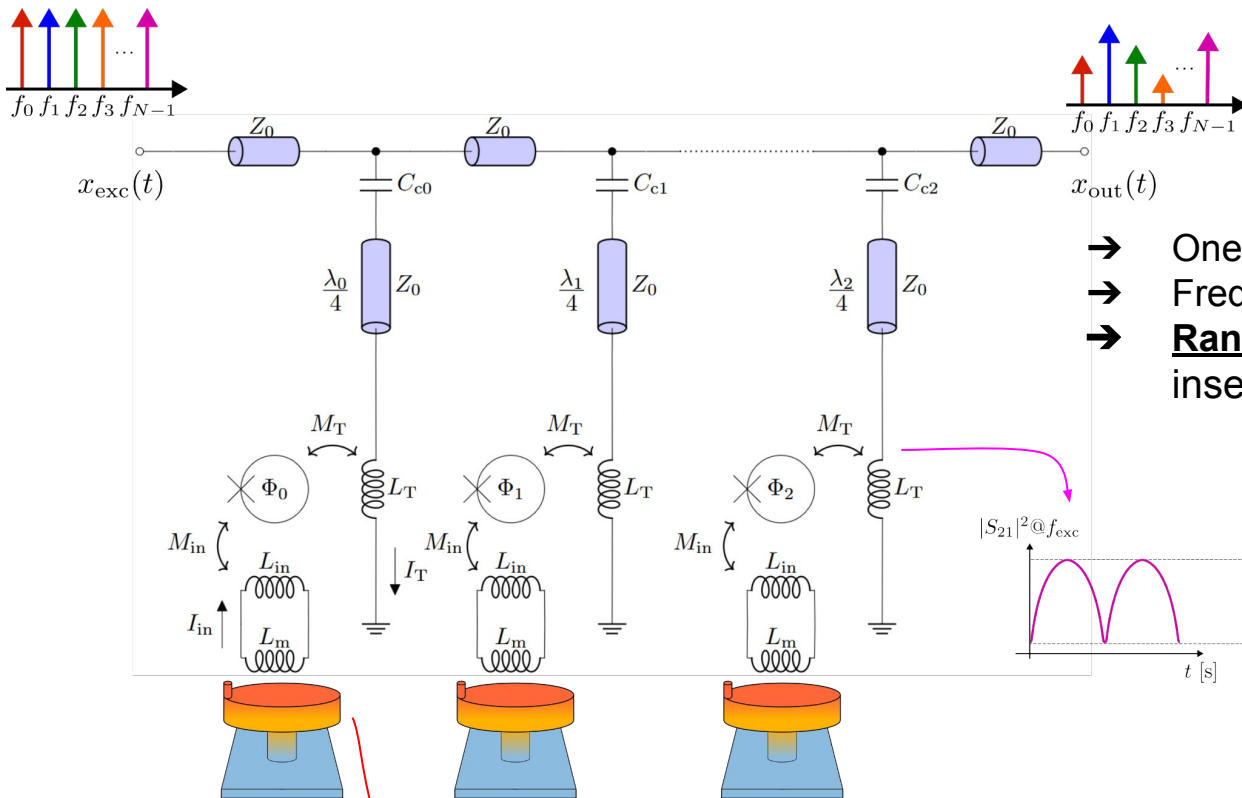


The Microwave SQUID Multiplexer

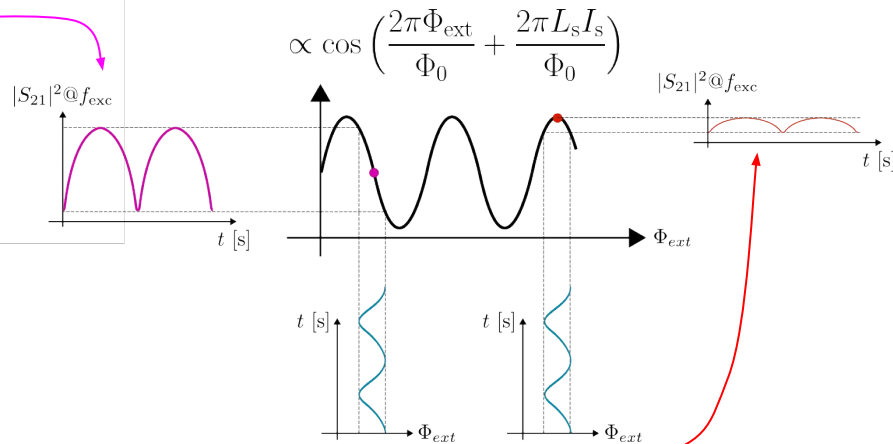


- One readout tone per channel
- Frequency division multiplexing

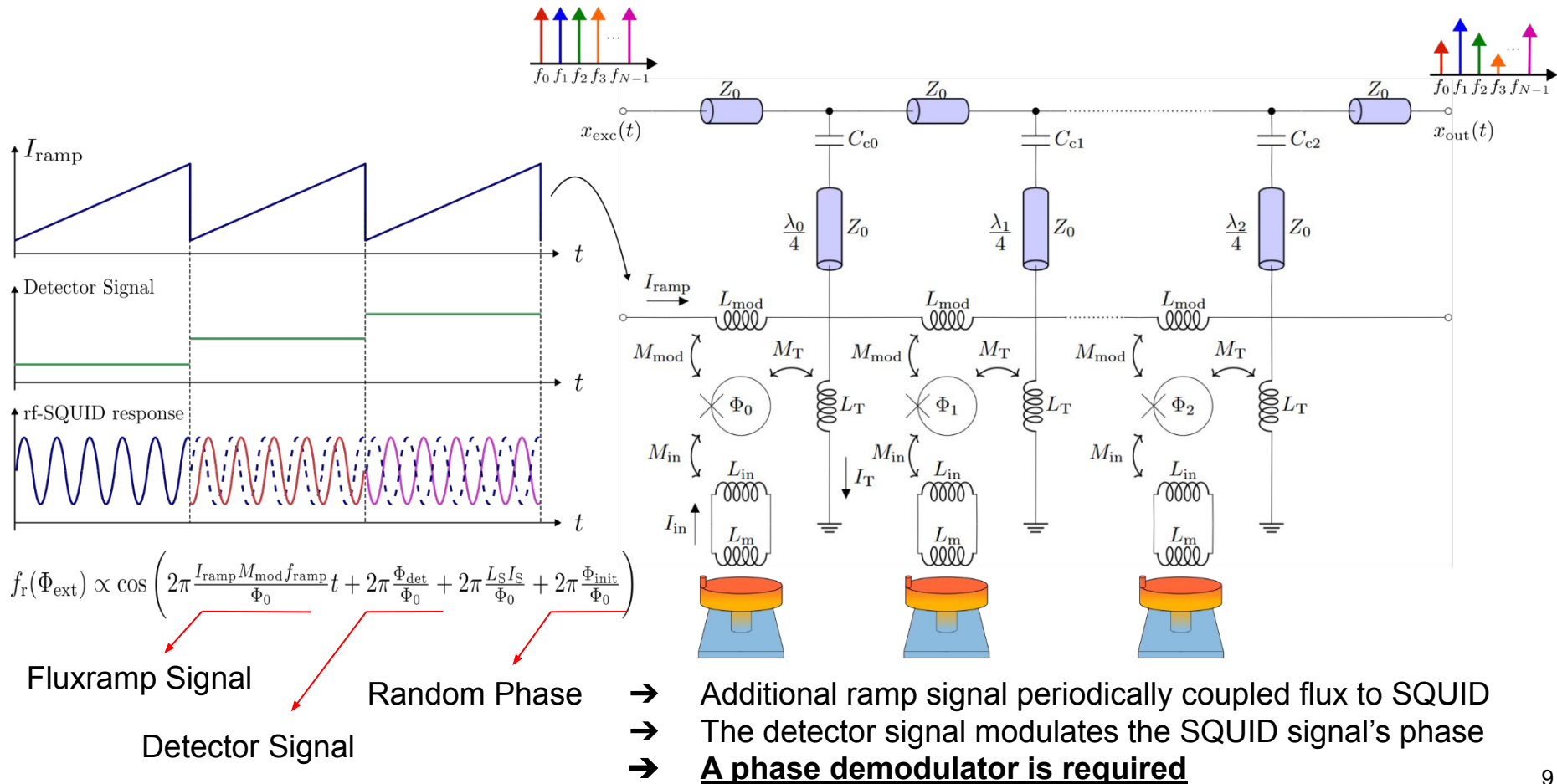
The Microwave SQUID Multiplexer



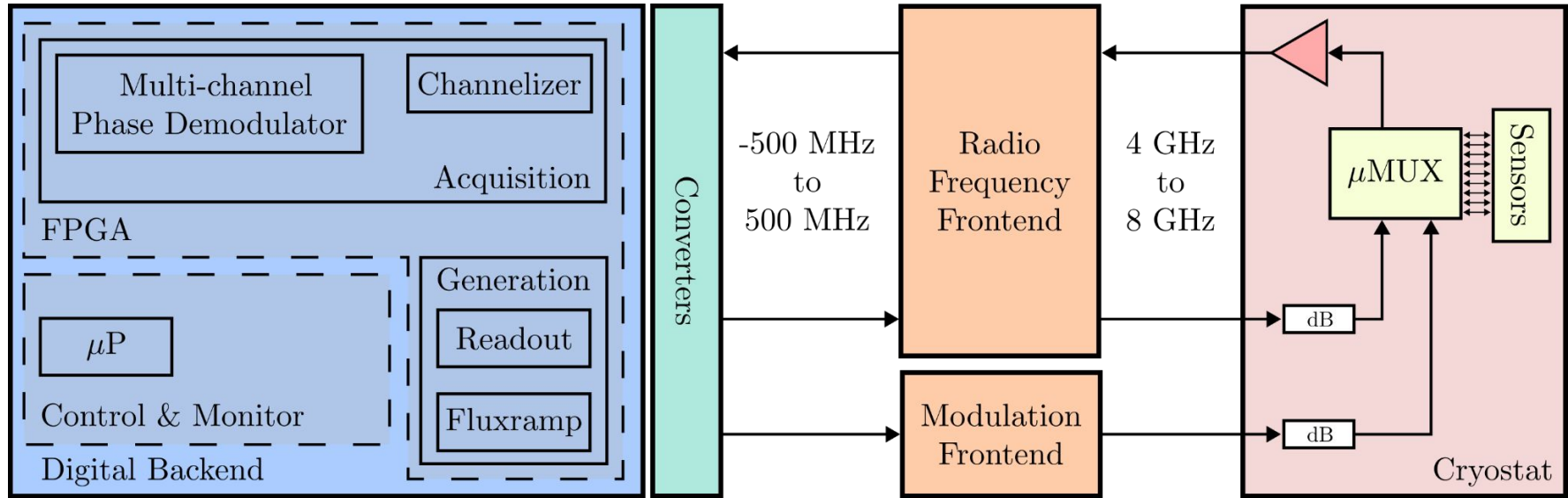
- One readout tone per channel
- Frequency division multiplexing
- **Random external flux problem:** insensitive SQUIDs



The μ MUX: Fluxramp modulation

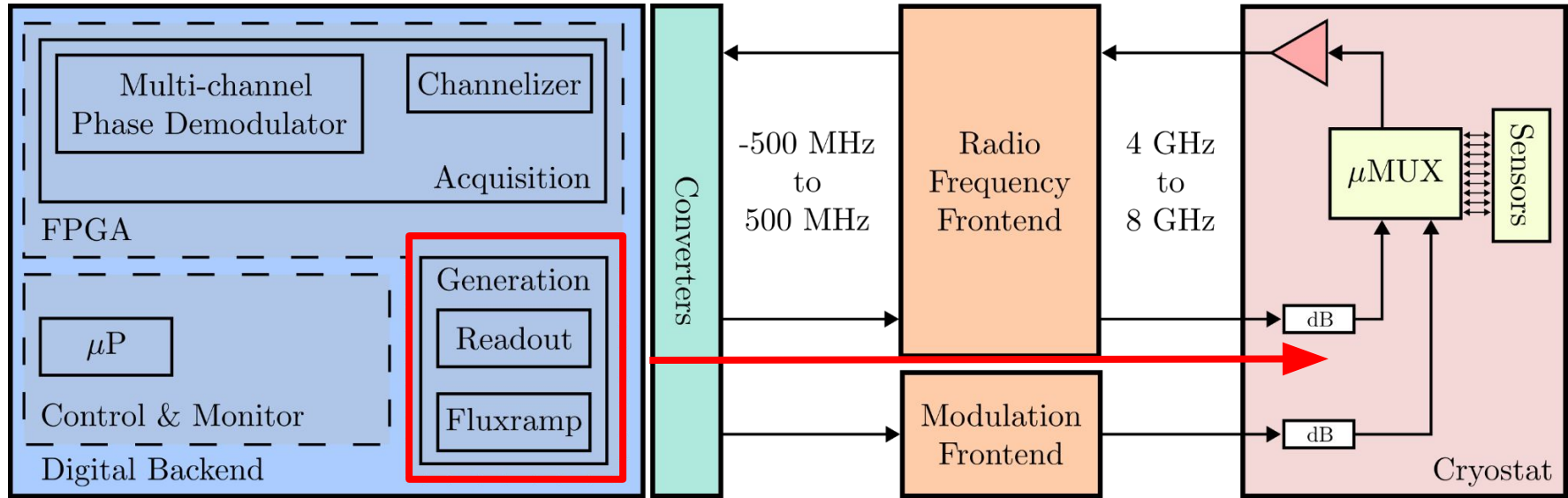


Software-defined radio scheme



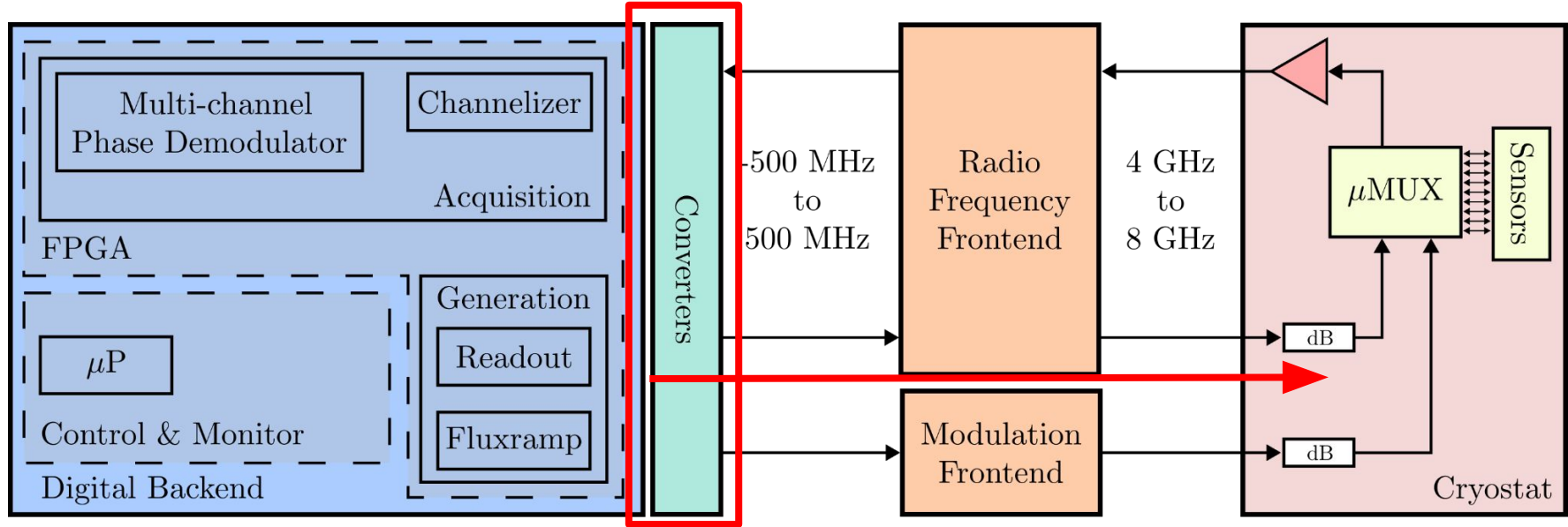
- Fluxramp and multi-tonal readout signals generation
- The readout tones are converted to analog by multiple DACs, each covering a complex bandwidth from -500 MHz to 500 MHz
- Readout signal up- and down-conversion from MHz to GHz band
- Signal acquisition and processing
 - ◆ Channelizer: signal sub-band splitting, filtering, down-sampling, and rf-SQUID recovery.
 - ◆ Fluxramp demodulation

Software-defined radio scheme



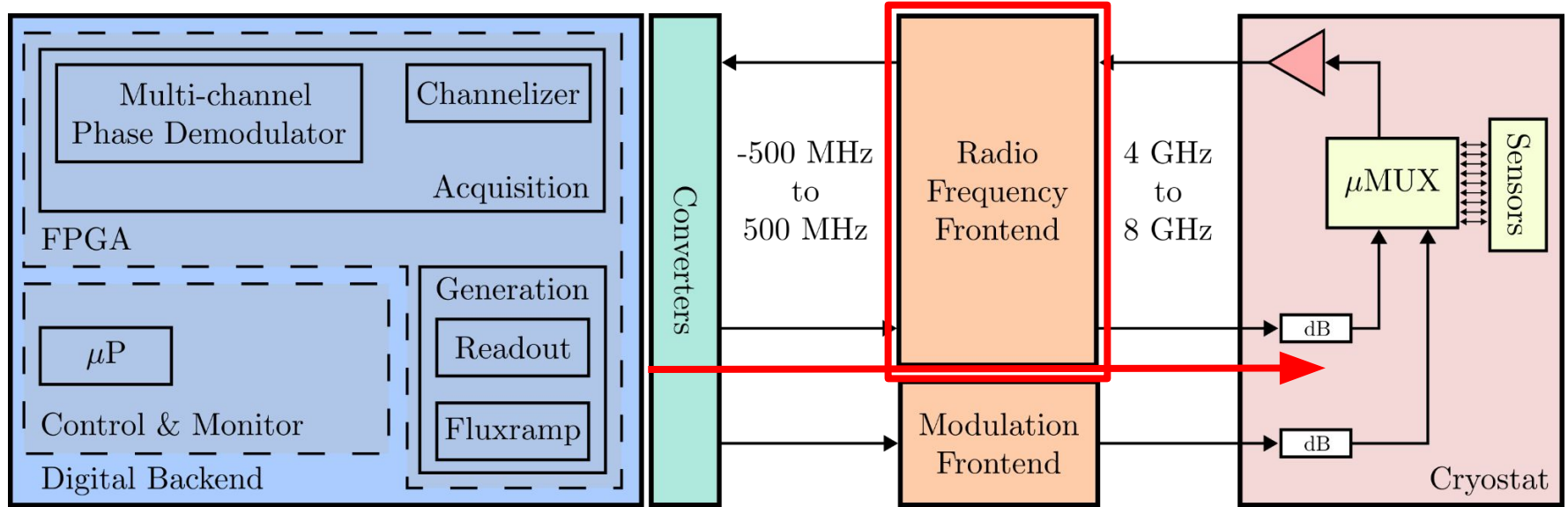
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Software-defined radio scheme



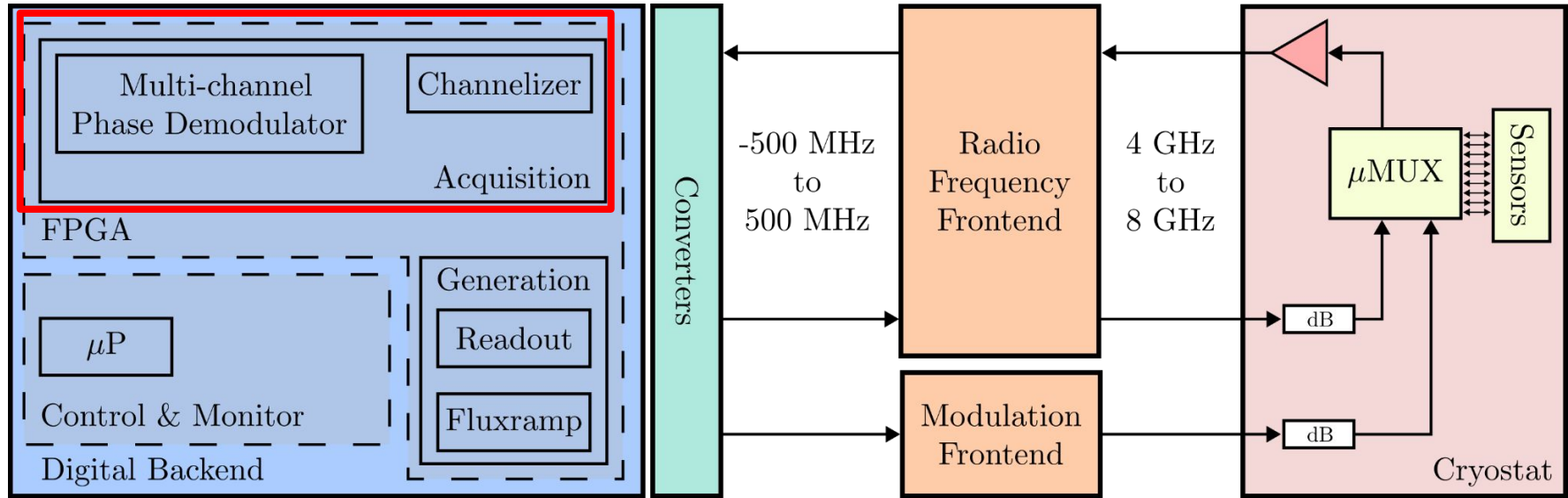
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Software-defined radio scheme



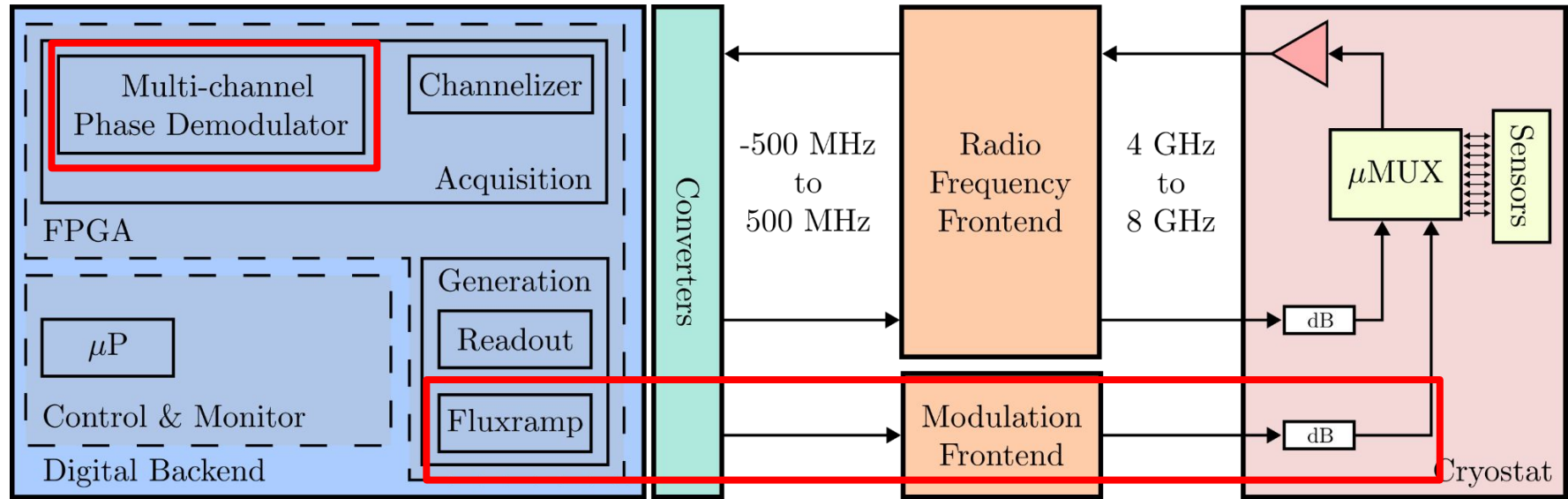
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Software-defined radio scheme



- Fluxramp and multi-tonal readout signals generation
- The readout tones are converted to analog by multiple DACs, each covering a complex bandwidth from -500 MHz to 500 MHz
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 - ◆ Fluxramp demodulation

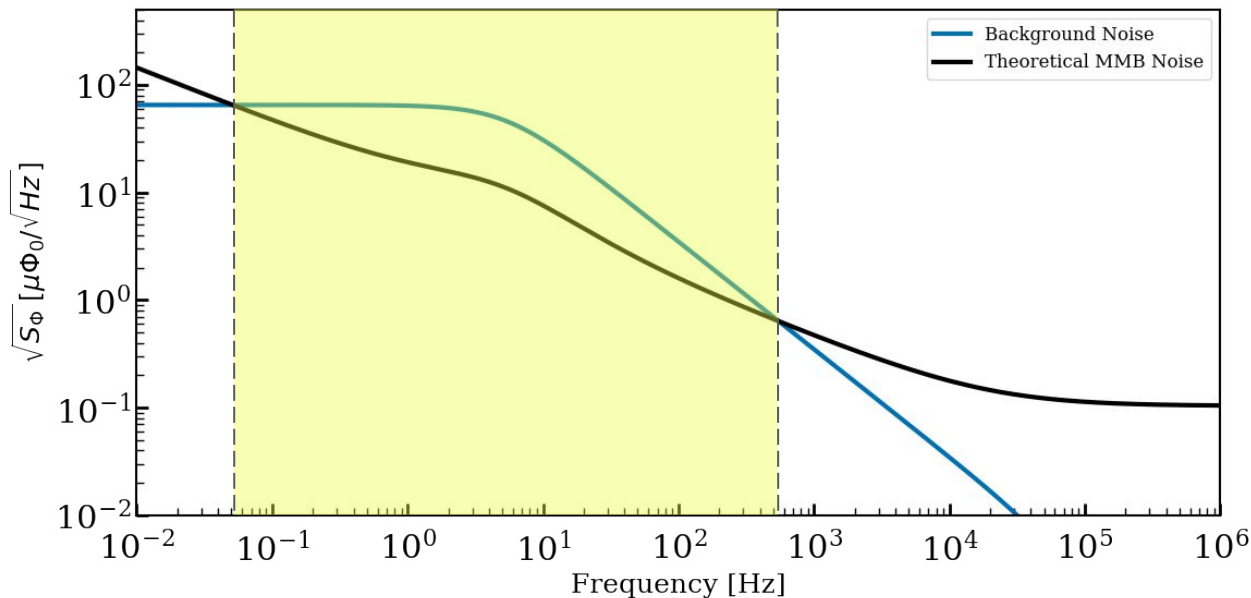
This work objectives



- Generation sub-system
 - ◆ **Fluxramp signal chain design**
 - ◆ **Integrate the signal generation system**
- Acquisition & Processing sub-system
 - ◆ **Demodulation of multichannel detector signals**
 - ◆ **Acquisition chain integration**
- Readout System Validation

Fluxramp signal noise requirement

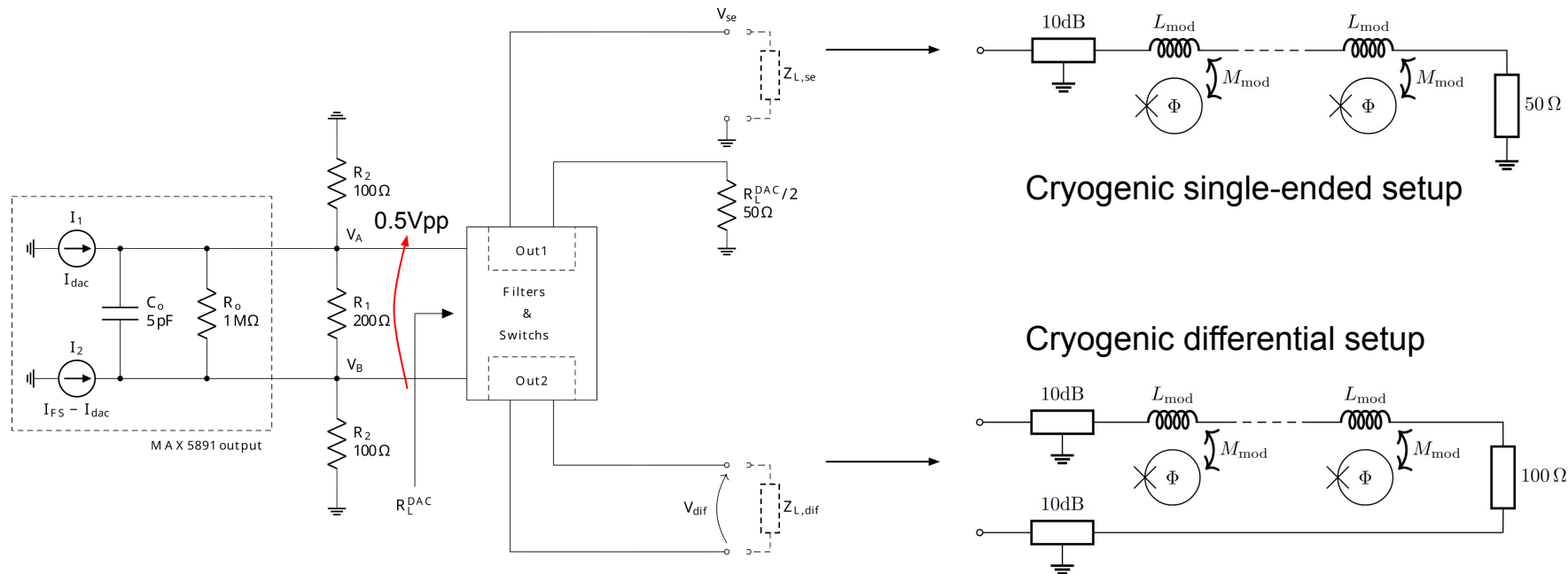
- Background noise > Detector noise > Readout noise
- Background Limited Photometry (BLIP) condition achieved from 0.045 Hz to 760 Hz



- Fluxramp noise much less than $0.6 \mu\Phi_0/\sqrt{\text{Hz}}$

MSS analog frontend

→ Modulation Signal Synthesizer (MSS) around the 16 bits DAC MAX5891



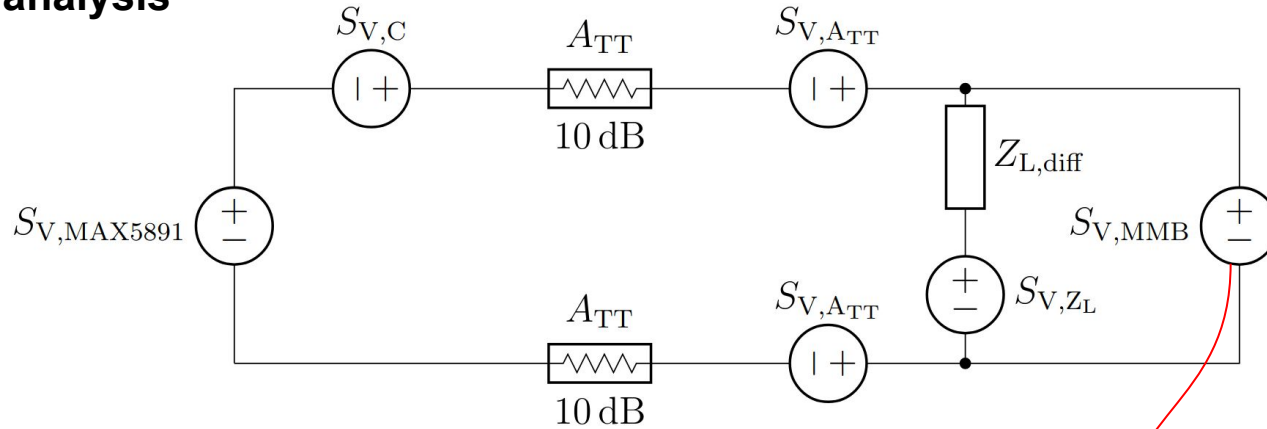
→ Theoretical noise spectral density $S_{MAX5891}|_{\text{dBm}} = 1\text{ dBm} - \text{SNR}_{\text{dB}} - 10 \log_{10} \left(\frac{f_s^{MAX5891}}{2} \right) = -164 \frac{\text{dBm}}{\text{Hz}}$

20mA full scale current in a double-terminated 100Ω load

10MHz clock signal

→ 10dB attenuation enables coupling of 1 to $8\phi_0$ and reduces fluxramp noise

MSS: Noise analysis



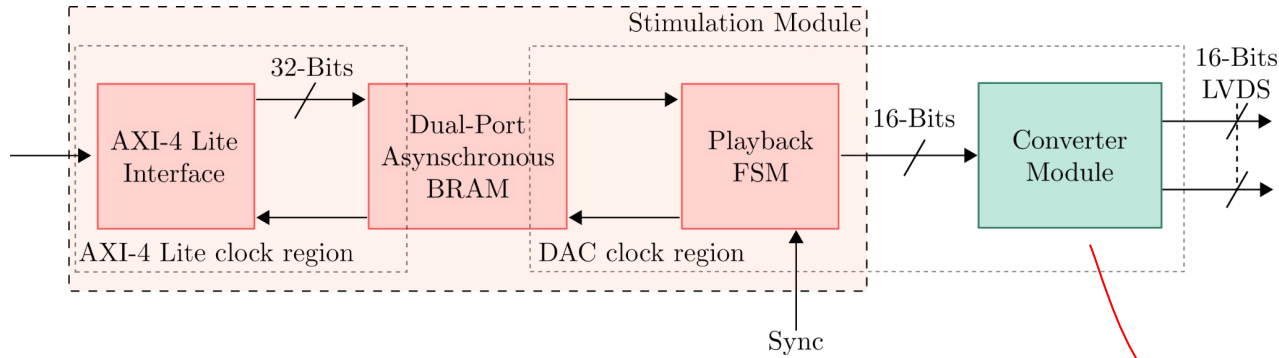
Source	Voltage Spectral Density (nV/ $\sqrt{\text{Hz}}$)
DAC quantized noise	0.630 (considering attenuator)
Current to voltage converter	0.204 (considering attenuator)
Cryogenic attenuator	0.053
MSS load	0.149
Total Noise	0.683

Modulation line coupling
($M_{\text{mod}} = 2291 \phi_0/A$)

$$S_{V,MMB} = \frac{\sqrt{S_{\Phi,MMB}}}{M_{\text{mod}}} \cdot 100 \Omega = 26.2 \frac{\text{nV}}{\sqrt{\text{Hz}}}$$

**MMB signal degraded
by 0.034%**

MSS digital backend

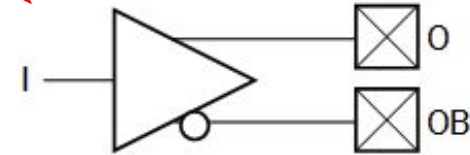


MPSoC ZCU102



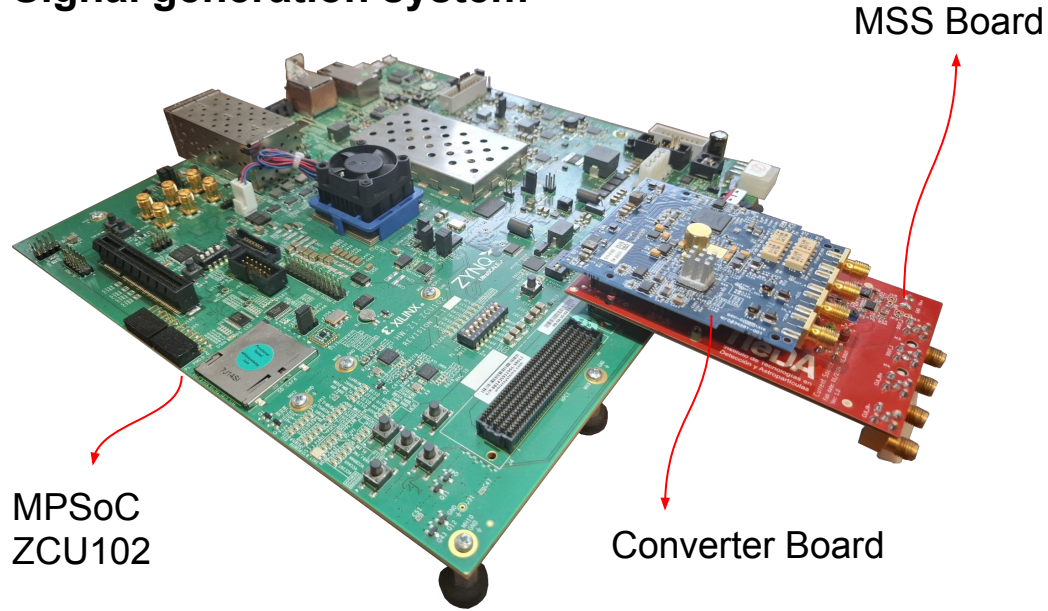
- MPSoC ZCU102 selected as digital backend
- Dual-port BRAM
 - ◆ Arbitrary waveform generation
 - ◆ Playback continuous signal
 - ◆ Real-time configuration using AXI-Lite protocol
- Synthesizable signal frequencies

$$\frac{f_{\text{clk}}}{L_{\text{bram}}} \geq f_{\text{out}} > \frac{f_{\text{clk}}}{2}$$



Differential Signaling Output Buffer

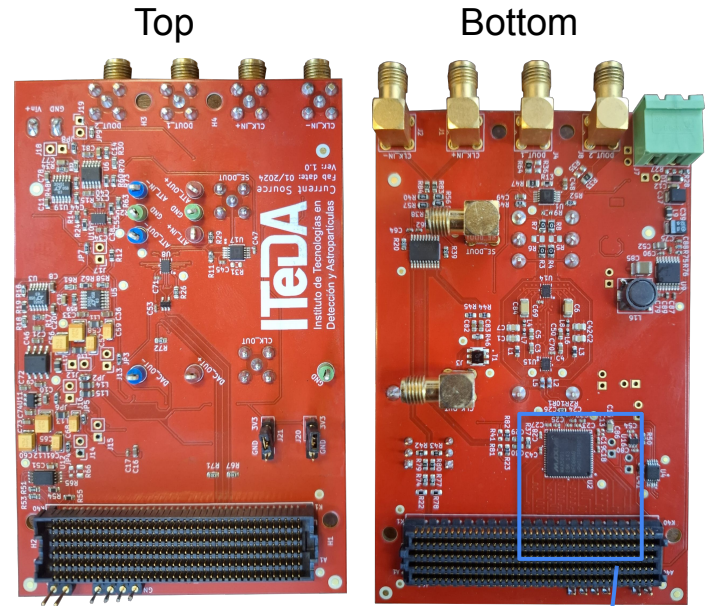
Signal generation system



MPSoC
ZCU102

Converter Board

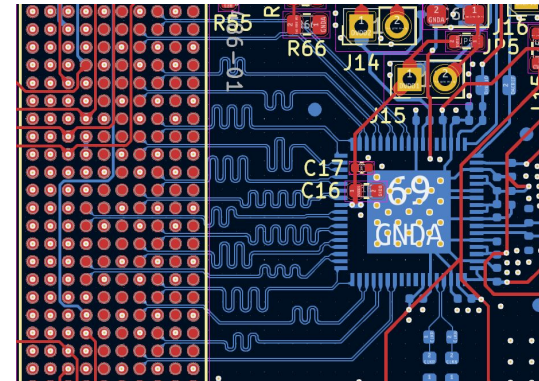
MSS Board



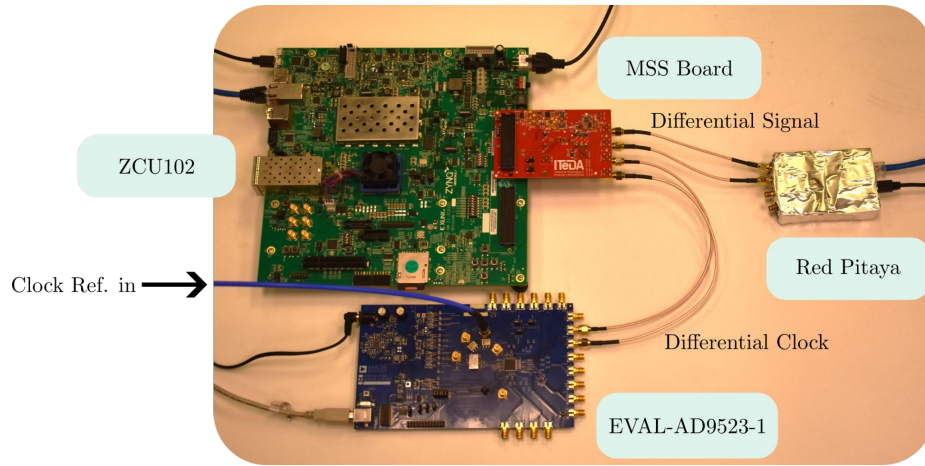
Top

Bottom

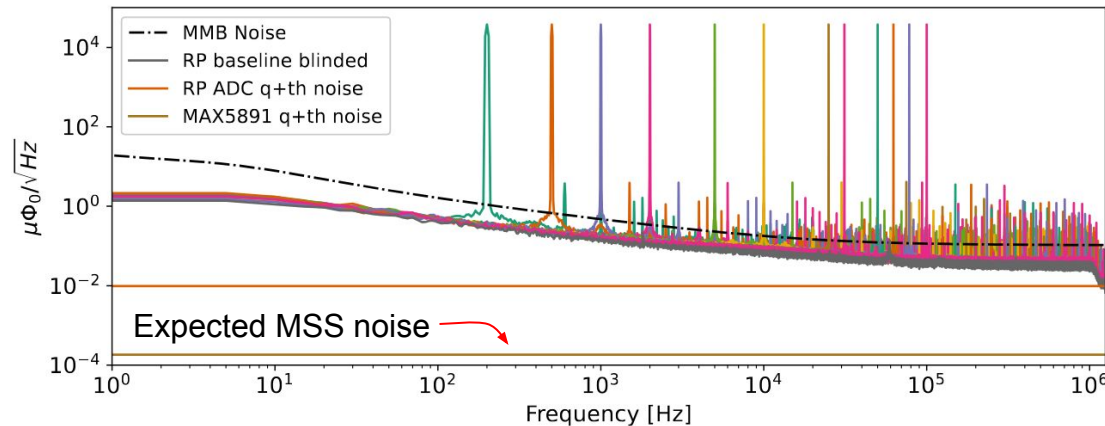
- Stackable board system (MPSoC-MSS-Converter board)
 - ◆ Dual high density FMC+ connector
 - ◆ Via-in-pad for FMC+ male-female connection
- 16 differential microstrip transmission lines
- Intra- and inter-line delay matching



MSS characterization

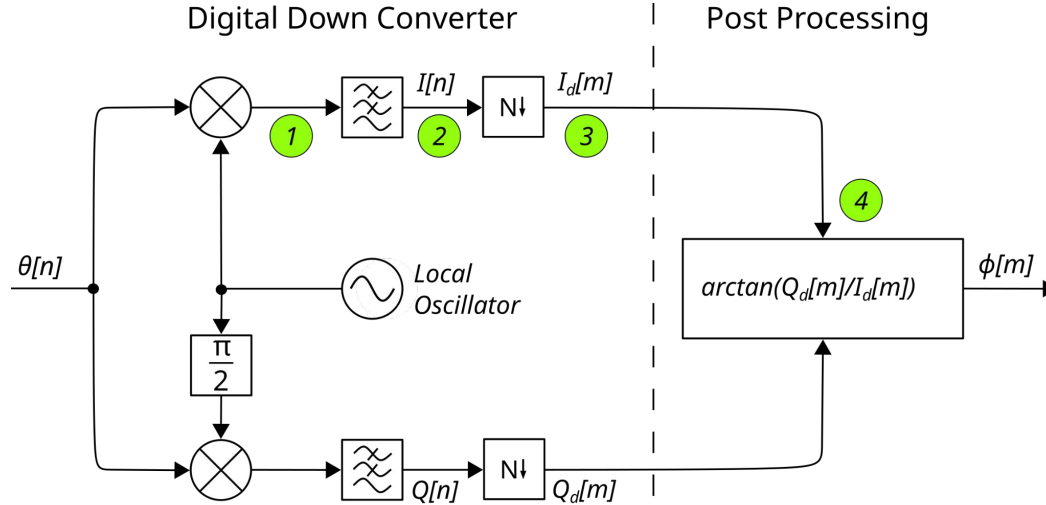


- Clock generated by the EVAL-AD9523-1 board
- Signal acquisition using Red Pitaya
- 200Hz to 100kHz signal generation
- Spurious free dynamic range (SFDR) and total harmonic distortion (THD) characterization
- SFDR=80dBc and THD < 0.02% consistent with specified in datasheet
- Red Pitaya noise is dominant (added 26dB gain amplifier)



Baseline noise below MMB noise

Multi-channel quadrature demodulator



$$\phi[m] = \arctan \left(\frac{\sum_{n=0}^{N-1} \theta[n] \sin(\Omega_{\text{mod}} n)}{\sum_{n=0}^{N-1} \theta[n] \cos(\Omega_{\text{mod}} n)} \right)$$

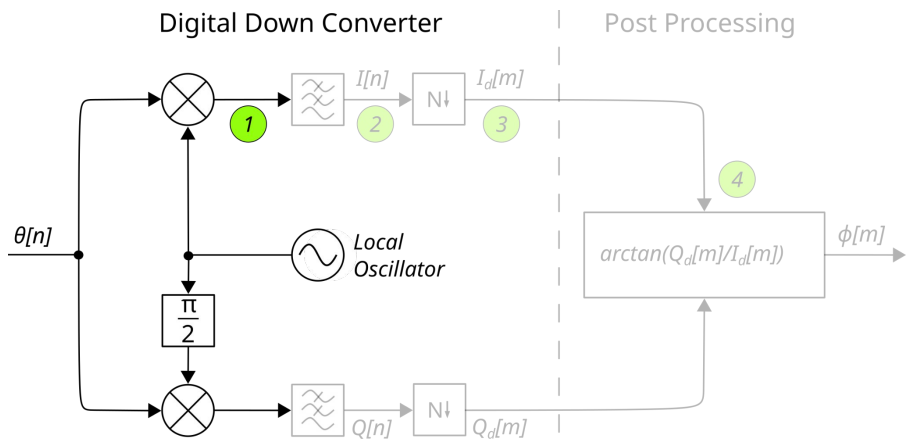
→ Correlation method with the rf-SQUID signal for phase demodulation

$$f_{\text{mod}} = \frac{I_{\text{ramp}} M_{\text{mod}}}{\Phi_0} f_{\text{ramp}}$$

→ Phase recover from the arctan function of the real and imaginary signal relation

→ Time-division Multiplexing (TDM) of multiple rf-SQUID signals through a buffer

Down-conversion implementation

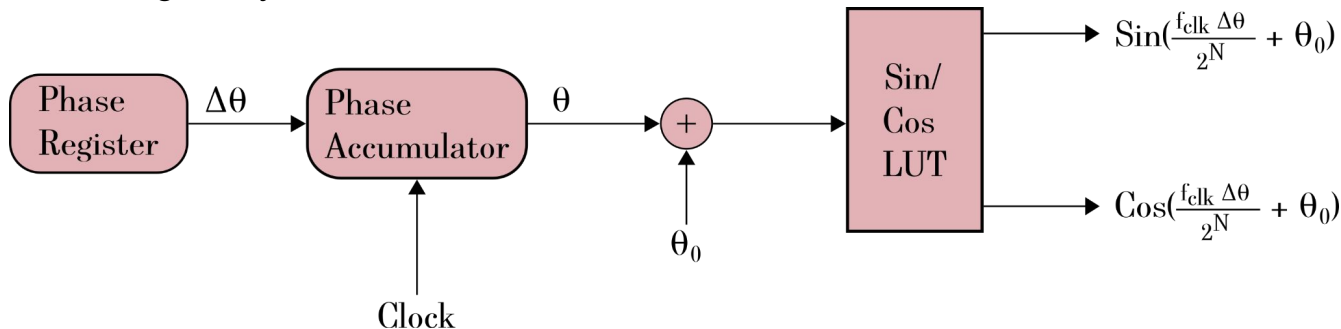


1

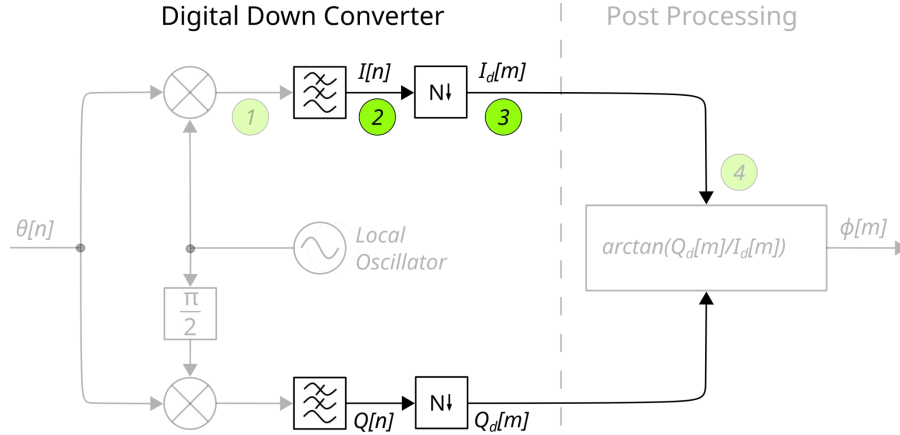
Down-conversion

- DSP slice for efficient multiplication
- Complex signal generated by a DDS
- A phase value is generated as the index for a memory preloaded with sine and cosine samples
- The phase value is generated by cyclically adding the Phase Register value to the Phase Accumulator
- θ_0 sets the initial phase
- One phase register for each input signal to be multiplexed in time

Direct Digital Synthesizer



Filter implementation



$$H(z) = \frac{b_0 + b_1 z^{-1} + b_2 z^{-2} + \dots + b_N z^{-N}}{1 + a_1 z^{-1} + a_2 z^{-2} + \dots + a_N z^{-N}}$$

General Digital Filter Form

$$\begin{aligned} a_x &= 0 \\ b_x &= 1 \end{aligned}$$

$$H(z) = 1 + z^{-1} + z^{-2} + \dots + z^{-N}$$

Average Filter

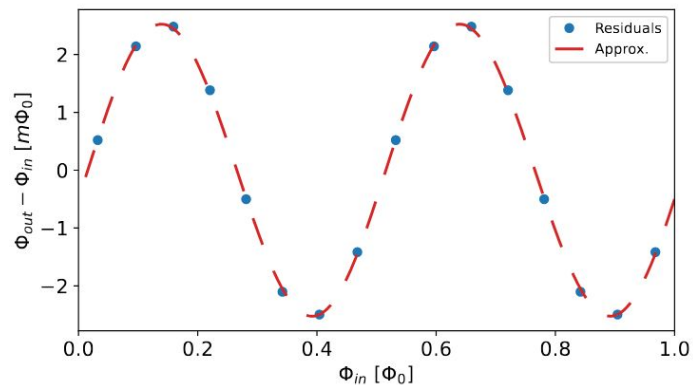
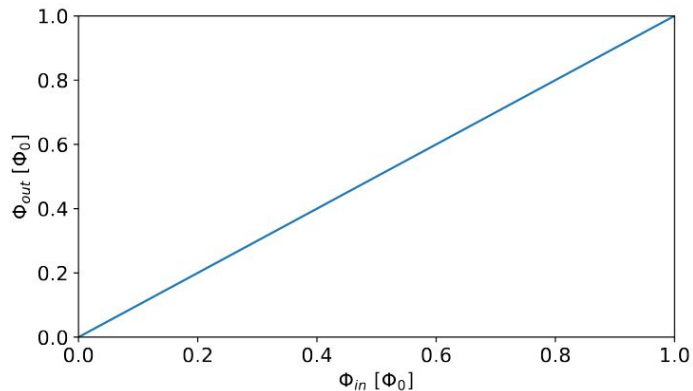
2 Filtering

- No multiplier needed
- Rectangular window function
- A buffer stores the sum of the N elements in the FPGA implementation

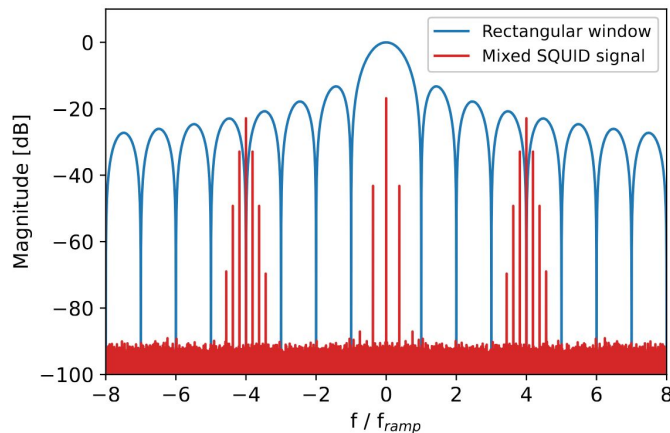
3 Downsampling

- One sample is output every N elements
- Spectral aliasing

Nonlinear error

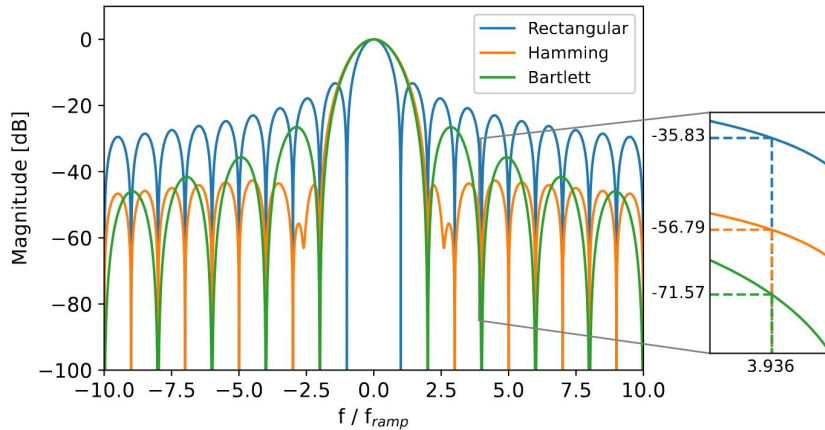


- Many groups reported non-linearities in the readout system
- Detector signal simulated as a linear signal
- Residuals observed at twice the detector signal frequency after the demodulator output
- **Conclusions: aliasing effects produced by the phase demodulator**



Weighted filter implementation

$$\phi[m] = \arctan \left(- \frac{\sum_{n=0}^{N-1} \theta[n] \sin(\Omega_{mod} n) W[n]}{\sum_{n=0}^{N-1} \theta[n] \cos(\Omega_{mod} n) W[n]} \right)$$



- Adding a window function improves the attenuation at the expense of higher FPGA resource usage
- An improvement of **more than 35dB** achieved with the Bartlett window
- **This work contributes with a publication**

Aliasing Effect on Flux Ramp Demodulation: Nonlinearity in the Microwave Squid Multiplexer

[Open access](#) | Published: 11 August 2023

Volume 213, pages 223–236, (2023) [Cite this article](#)

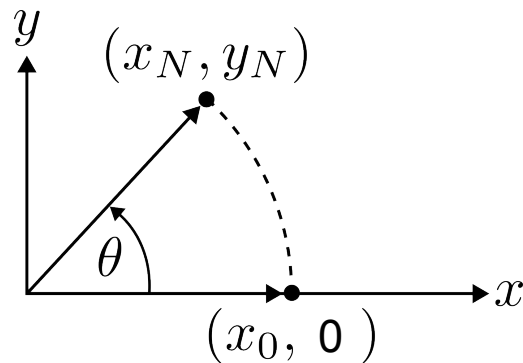
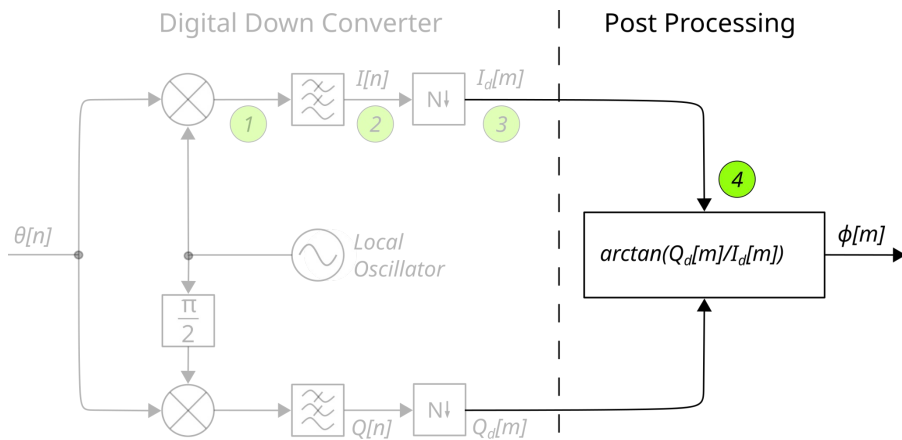
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Arctan implementation

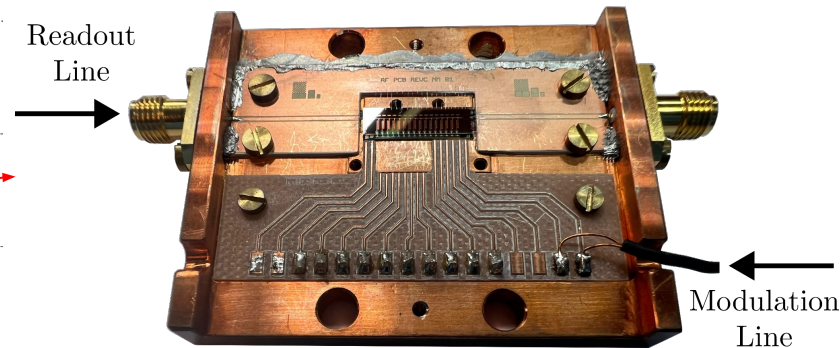


$$x[n+1] = x[n] - d[n] \cdot 2^{-n} \cdot y[n]$$

$$y[n+1] = y[n] - d[n] \cdot 2^{-n} \cdot x[n]$$

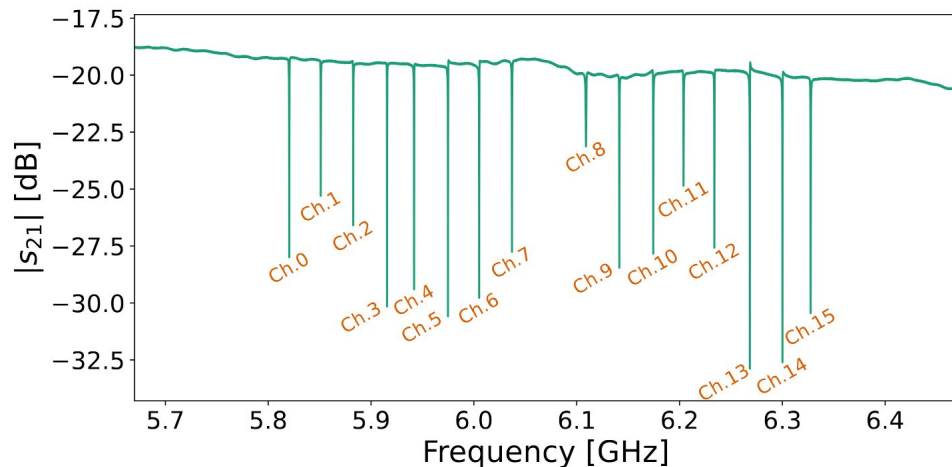
4 CORDIC algorithm

- Hardware efficient: requires only additions, subtractions and binary shifts
- A starting vector $(x_0, 0)$ is iteratively rotated to the angle corresponding to $\arctan(y_N/x_N)$
- The accumulated sum of the rotated angles provides the final result for the arctangent
- Adjustable precision: number of iterations determines the precision of the result

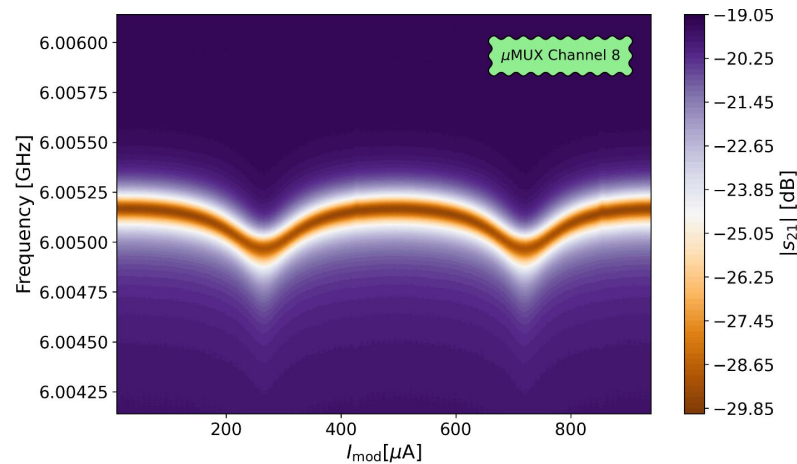


- 24

μ MUX characterization

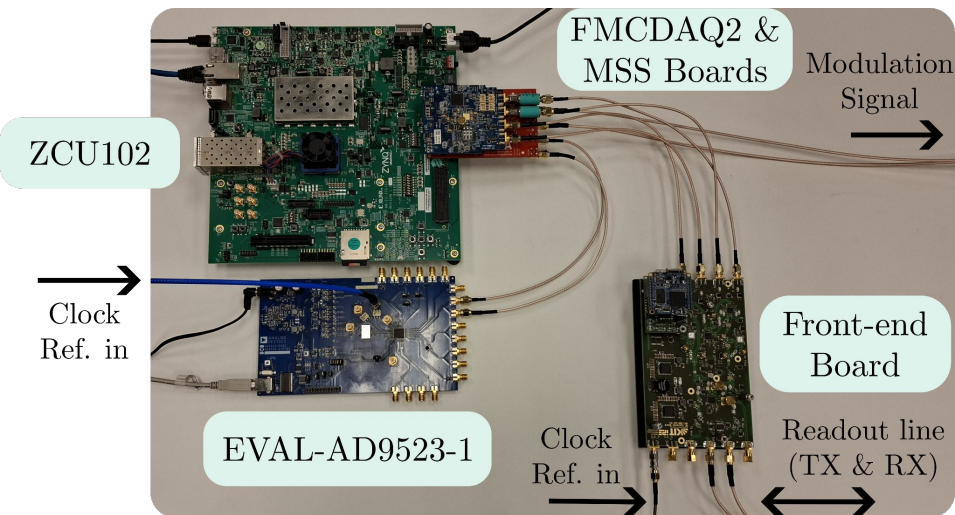


- μ MUX channel measurement using commercial VNA and no modulation signal
- Obtained channel parameters:
 - ◆ Resonance frequencies
 - ◆ Bandwidths
 - ◆ Transmission depths

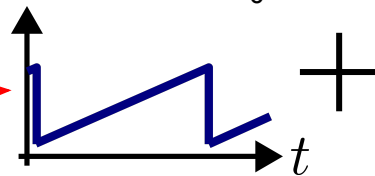


- Adding a DC current to the modulation line
- Swept over two SQUID periods
- Resonator response as a function of the flux signal
- M_{mod} calculated

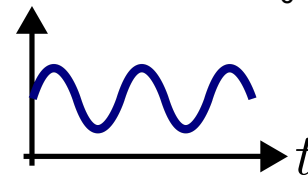
System integration and validation



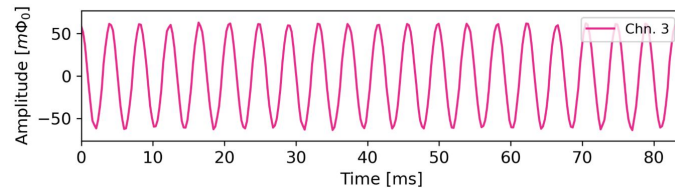
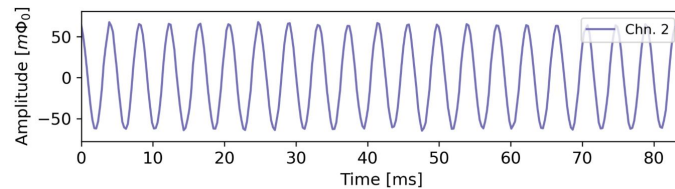
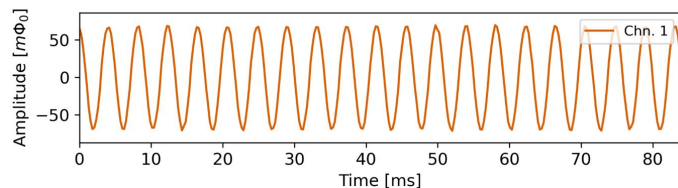
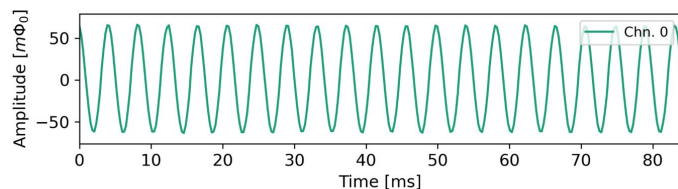
Fluxramp
3814Hz, $4\phi_0$



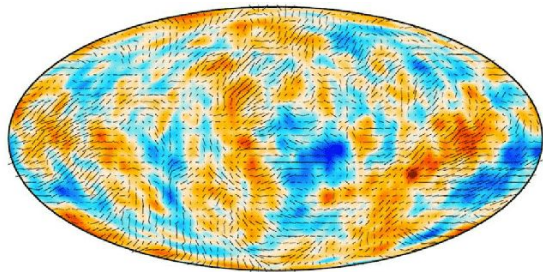
Emulated MMB
238Hz, $125m\phi_0$



- Multi-channel quadrature demodulator integrated with a 4-channel channelizer.
- Complete readout assembly
- A 238 Hz, 125 $m\phi_0$ MMB signal was emulated (added to the modulation signal in the BRAM)
- **Successful detector signal demodulation**

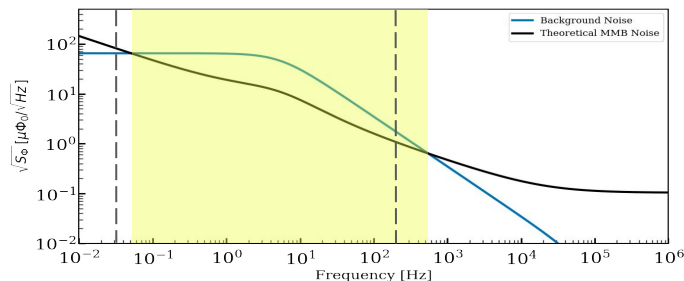


Summary



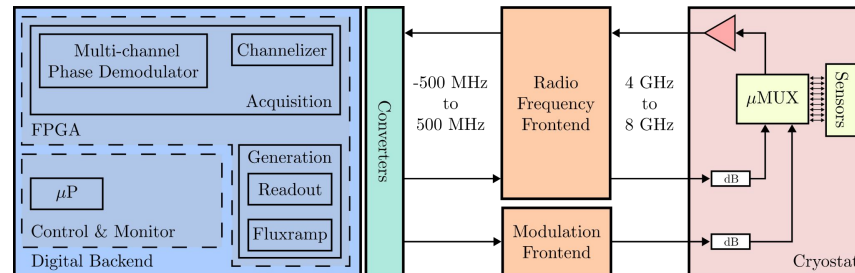
Scientific motivation

B-modes detection for inflation theory validation



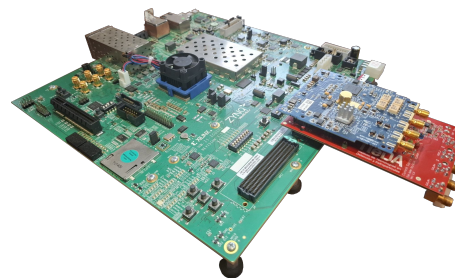
Experimental requirement

Integrated readout system
Background limited photometry



Experimental strategy

Bolometric interferometry, Magnetic Microbolometer,
Microwave SQUID Multiplexer, Software-defined radio

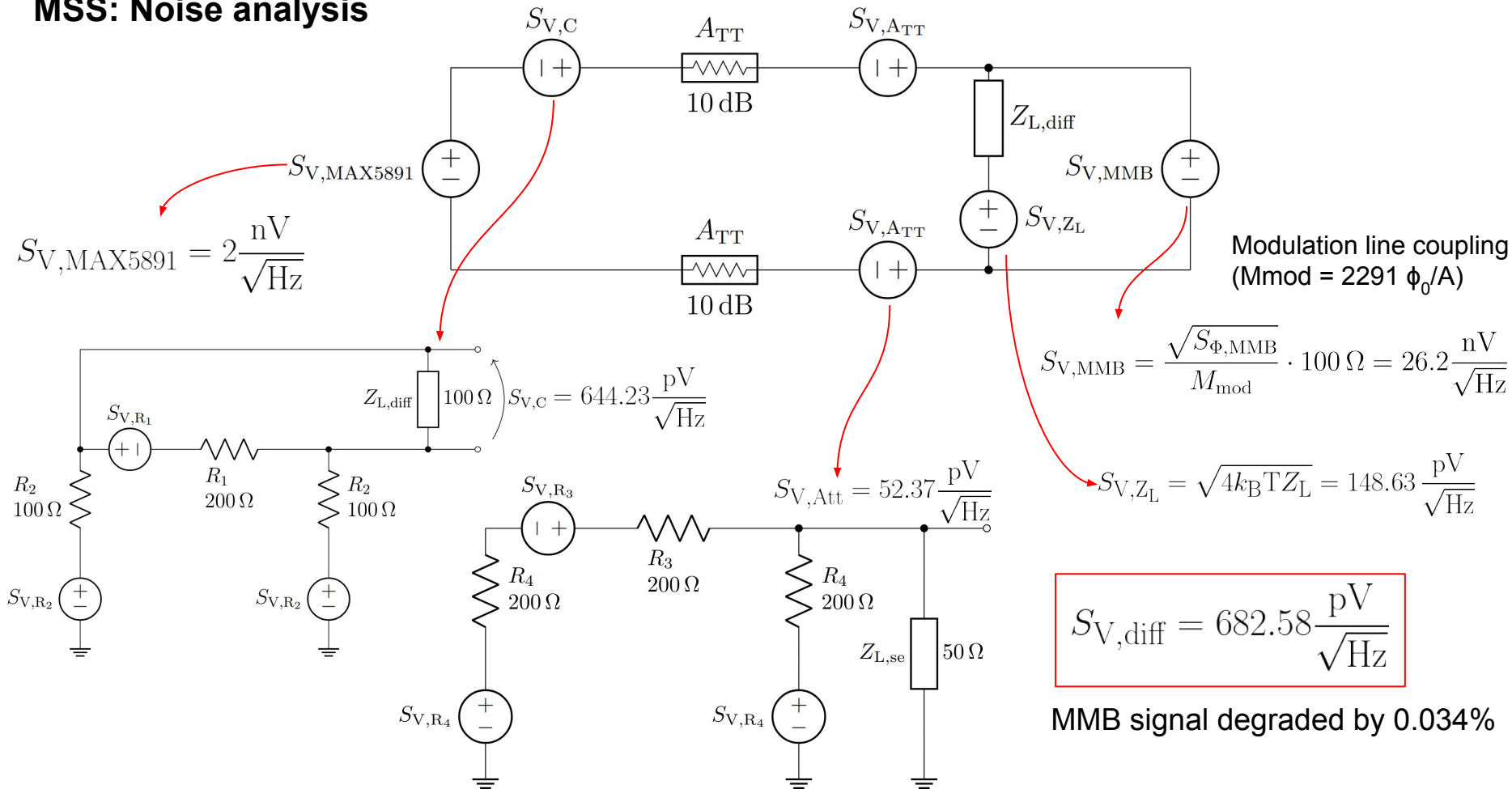


Contributions

Integrated signal generation sub-system
Integrated acquisition & processing sub-system
Proposal for aliasing effect mitigation

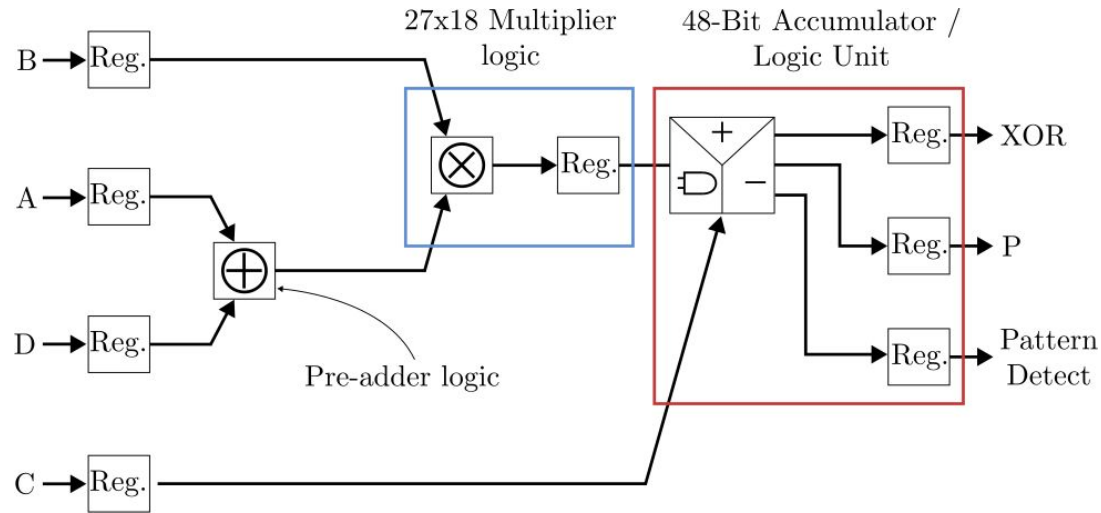
Back-up

MSS: Noise analysis



Multiplication implementation

1 Multiplier



- Intellectual Property Core DSP48E2
- Specialized block for efficient multiplication and accumulation (MAC operations)

Background noise

$$\text{NEP}_{\gamma}^2 = 2hfP_{\text{opt}} + \frac{2P_{\text{opt}}^2}{m\Delta f}$$

Center frequency

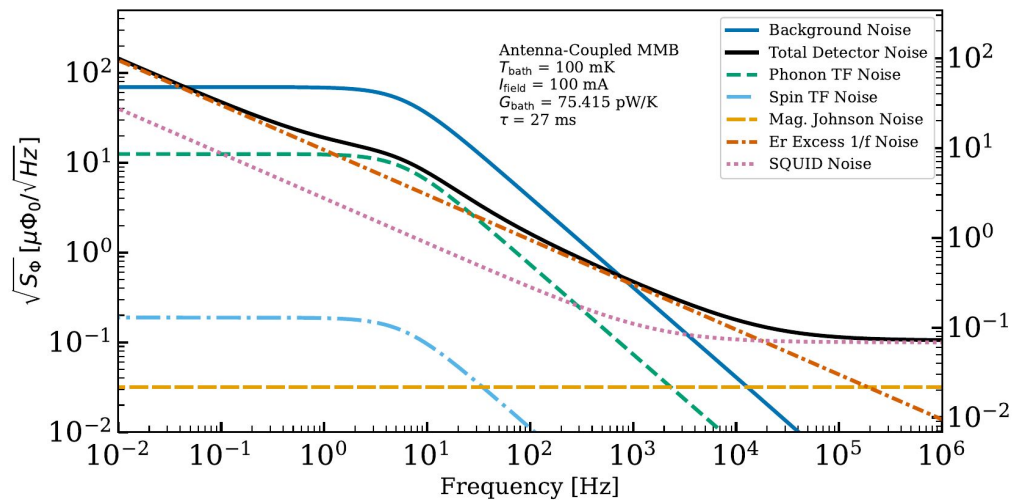
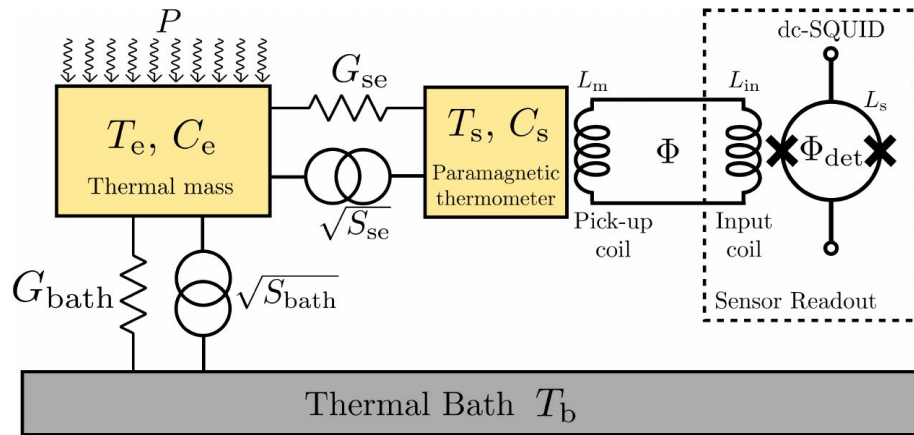
Signal power
absorber by the MMB

Bandwidth

The diagram illustrates the components of the equation for the squared Noise Equivalent Power (NEP_γ²). Red arrows point from the following labels to their corresponding terms in the equation:

- Center frequency** points to the frequency f in the term $2hfP_{\text{opt}}$.
- Signal power absorber by the MMB** points to the optimal power P_{opt} in the term $2hfP_{\text{opt}}$.
- Bandwidth** points to the bandwidth Δf in the denominator of the second term $\frac{2P_{\text{opt}}^2}{m\Delta f}$.

MMB noise



Fluxramp demodulator implementation

